

# ALTEC SERVICE COMPANY



Many Ancient Transformers, A Few Amplifiers, Alignment Of Built-In Equalization, 1936.. 1945.. 1948.. And More

SCANNED BY PATRICK JANKOWIAK KD5OEI

COLOR CODE: ALTEC WESTERN ELECTRIC RESTRICTED

WESTERN ELECTRIC

*In order of appearance...*

	DOCUMENT DESIGNATION
ALTEC LANSING OUTPUT TRANSFORMER CHART 3753	50.48
ALTEC LANSING AND WESTERN ELECTRIC SPEECH TRANSFORMER CHART 3756	50.48
EQUALIZING NETWORKS AND CURVES	40.64
ALTEC LANSING MATCHING TRANSFORMER CHART 3754	50.48
ALTEC LANSING POWER TRANSFORMER CHART 3757	50.48
ALTEC LANSING CHOKE COIL CHART 3755	50.48
WESTERN ELECTRIC POWER TRANSFORMER CHART 1936 RESTRICTED	4.48
WESTERN ELECTRIC OUTPUT TRANSFORMERS AND REPEATING COILS CHART 1936 RESTRICTED	4.48
WESTERN ELECTRIC INPUT TRANSFORMERS CHART 1936 RESTRICTED	4.48
ALTEC LANSING POWER AMPLIFIER A-126	50.03
ALTEC LANSING POWER AMPLIFIER EQUALIZING A-126	50.03
ALTEC LANSING POWER AMPLIFIER SCHEMATIC AND EQUALIZER A-126/A/B DRAWING 3885	50.03
ALTEC LANSING POWER AMPLIFIER SCHEMATIC A-126 FOR LOWE'S EMERGENCY SYSTEM MODDED PER AS-1734 AX-1634	50.38
ALTEC LANSING POWER AMPLIFIER SCHEMATIC A-126 FOR LOWE'S EMERGENCY SYSTEM MODDED PER AS-1734 WITH A-442 PREAMP MODIFIED PER AQ-1686 AX-1635	50.38
EQUALIZER CHARACTERISTICS (PARTIAL) A-126 AMPLIFIER WITH SIMPLIFIED EQUALIZER DWG AQ-1936	50.03
WESTERN ELECTRIC 91 AMPLIFIER CHARACTERISTICS DWG AQ-8337-A	4.64
WESTERN ELECTRIC 91 AMPLIFIER CHARACTERISTICS DWG AQ-8337-B	4.64
AND FOLLOWS MORE EQUALIZATION CURVES ...	
TWO-TERMINAL R-C EQUALIZER DESIGN	4.64
THE DESIGN OF ATTENUATOR NETWORK	4.64





SPEECH TRANSFORMERS, GENERAL

ALTEC SERVICE CORPORATION

TYPE	APPLICATION	BALANCED TO GROUND	ALTEC LANSING TRANSFORMERS - SPEECH						FREQ. RANGE	RESPONSE	MAX. LEVEL REFW.	SHIELDING	OVERALL DIMENSIONS AS MOUNTED. (INCHES)	MOUNTING DIMENSIONS (INCHES)
			INPUT		OUTPUT		CONDUCT TO STRAP	CONDUCT TO STRAP						
			OHMS	STRAP	OHMS	STRAP								
TB-101	INPUT - LINE TO SINGLE OR PP GRIDS	SECONDARY ONLY	500 125	1-4 1-4	2-3 1-3,2-4	70,000 17,500	5-8 5-8	6-7 9-7,8-8	20- 20000	1 DB	-20 DB	25 DB MAGNETIC & ELECTROSTATIC	1 3/4 x 1 3/8 DIA	1 1/2
TB-102	INPUT - LINE TO SINGLE OR PP GRIDS	SECONDARY ONLY	250 125 62.5	1-6 2-5 1-5	3-4 3-4 1-4,3-4,5	70,000 17,500	7-10 7-10	8-9 7-9,8-10	20- 20000	1 DB	-20 DB	25 DB MAGNETIC & ELECTROSTATIC	1 3/4 x 1 3/8 DIA.	1 1/2
TB-103	INPUT - LINE TO SINGLE OR PP GRIDS	SECONDARY ONLY	500 250 125	1-3 1-3 2-3	2-5 2-5	70,000 17,500	5-8 3-8	6-7 9-7,8-8	20- 20000	1 DB	-20 DB	25 DB MAGNETIC & ELECTROSTATIC	1 3/4 x 1 3/8 DIA.	1 1/2
TB-104	INTERSTAGE ON BRUSHES SINGLE OR PP PLATES TO SINGLE OR PP GRIDS	PRIMARY & SECONDARY	10000 2500	1-4 1-4	2-3 1-3,2-4	40,000 10,000	7-10 7-10	8-9 7-9,8-10	20- 20000	1 DB	-20 DB	25 DB MAGNETIC & ELECTROSTATIC	1 3/4 x 1 3/8 DIA.	1 1/2
TBA-105 (WE-233E)	INPUT - LINE TO GRID	NO	500 250	1-6 1-6	2-5 2-6,1-5	25,000 6,250	3-8 3-8	4-7 3-7,4-8	60- 8000	0.50B	+12 DB	30 DB	3 1/2 x 2 1/8 x 5 1/8 H	2 3/8 x 2 3/8
TBA-106 (WE-247A)	INPUT - LINE TO GRID	NO	250	1-4	2-3	150,000	5-6		60- 8000	0.5 DB	+4 DB	30 DB	2 1/2 x 2 1/8 x 3 1/8 H	2 3/8 x 2 3/8
TBA-201A (WE-2470A)	INPUT - REC TO LINE	NO	50000	BL-BL	WH	25	RD-RD	WH	100- 6000	1 DB	0 DB	25 DB	1 1/2 x 1 3/8 DIA.	
TBB-101	INPUT - LINE TO SINGLE OR PP GRIDS	SECONDARY ONLY	500 125	1-4 1-4	2-3 1-3,2-4	70,000 17,500	7-10 7-10	8-9 7-9,8-10	20- 20000	1 DB	-20 DB	30 DB MAGNETIC & ELECTROSTATIC	2 1/2 x 2 3/8 x 2 3/8 H	1 7/8 x 1 7/8
TBB-102	INPUT - LINE TO SINGLE OR PP GRIDS	SECONDARY ONLY	250 125 62.5	1-6 2-5 1-5	3-4 3-4 1-4,3-4,5	70,000 17,500	7-10 7-10	8-9 7-9,8-10	20- 20000	1 DB	-20 DB	30 DB MAGNETIC & ELECTROSTATIC	2 1/2 x 2 3/8 x 2 3/8 H	1 7/8 x 1 7/8
TBB-103	INPUT - LINE TO SINGLE OR PP GRIDS	SECONDARY ONLY	500 250 125	1-3 1-3 2-3	2-5 2-5	70,000 17,500	7-10 7-10	8-9 7-9,8-10	20- 20000	1 DB	-20 DB	30 DB MAGNETIC & ELECTROSTATIC	2 1/2 x 2 3/8 x 2 3/8 H	1 7/8 x 1 7/8
TBB-104	INPUT - LINE TO SINGLE OR PP GRIDS	SECONDARY ONLY	250 125 62.5	1-6 2-5 1-5	3-4 3-4 1-4,3-4,5	70,000 17,500	7-10 7-10	8-9 7-9,8-10	20- 20000	1 DB	-20 DB	30 DB MAGNETIC & ELECTROSTATIC	2 1/2 x 2 3/8 x 2 3/8 H	1 7/8 x 1 7/8
TBB-105	INTERSTAGE ON BRUSHES SINGLE OR PP PLATES TO SINGLE OR PP GRIDS	PRIMARY & SECONDARY	10000 2500	1-4 1-4	2-3 1-3,2-4	40,000 10,000	7-10 7-10	8-9 7-9,8-10	20- 20000	1 DB	-20 DB	30 DB MAGNETIC & ELECTROSTATIC	2 1/2 x 2 3/8 x 2 3/8 H	1 7/8 x 1 7/8
TBD-104 (WE-261B)	INPUT - LINE TO GRID	PRIMARY ONLY	200 50	1-4 1-4	2-3 1-3,2-4	110,000	5-6		20- 20000	1.50B	-20 DB	30 DB MAGNETIC & ELECTROSTATIC	2 1/2 x 2 3/8 x 5 1/8 H	2 3/8 x 2 3/8
TJ-102-A	INTERSTAGE ON OUTPUT PP WITH TERTIARY	PRIMARY & SECONDARY	2500 1375	1-4 1-4	2-3 1-3,2-4	3000 2000 1500 500	5-10 5-10 5-10 5-10	7-8 7-8 7-10 5-9,8-9	20- 20000	1 DB	+39 DB	NONE	4 x 4 5/8 x 5 1/8 H	3 1/2 x 4
TL-101 B	INPUT - A 287 F AMPL.	YES	500 250 125 62.5	1-6 2-5 1-5 1-5	3-4 3-4 1-4,3-4,5 1-4,3-4,5	30000	7-10	6-9	20- 20000	1 DB	+34 DB	NONE	3 1/2 x 3 3/8 x 4 1/8 H	2 3/8 x 2 3/8
TM-101 A (WE-264 C)	INTERSTAGE - SINGLE PLATE TO PP GRIDS	PRIMARY & SECONDARY	20000	1-2		100000	3-6	4-5	40- 8000	1 DB	20V PEAK ACROSS PRIMARY	30 DB MUM BUCKING	2 1/8 x 2 1/8 x 3 1/2 H	2 3/8 x 2 3/8
TMB-106	SPECIAL SERVICE DUAL WINDINGS	NO	50000	1-2 OR 6-7		1,000,000	3-5 OR 6-10	C.T. 5 4 8 9	20- 300	1 DB	2.5 V ACROSS PRIMARY	NONE		
TR-105	LOW LEVEL INPUT	NO	5000	RD,WH-RD		250,000	GRN-BLK		20- 10,000	2 DB	0 DB	NONE	1 3/8 DIA x 1 3/8 H	1 1/2

PRINTED IN U.S.A.

1	ADD	REVISION	DATE	BY	REASON
2	ADD	REVISION	DATE	BY	REASON
3	ADD	REVISION	DATE	BY	REASON
3A	ADD	REVISION	DATE	BY	REASON
3B	ADD	REVISION	DATE	BY	REASON
3C	ADD	REVISION	DATE	BY	REASON
3D	ADD	REVISION	DATE	BY	REASON

ALTEC LANSING CORPORATION  
MILLWOOD, CALIFORNIA

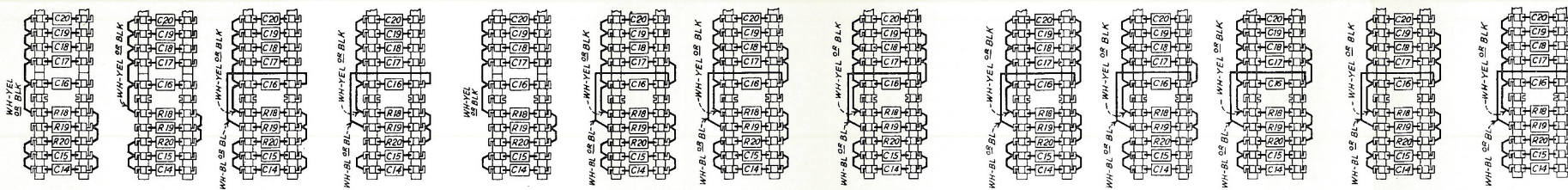
**SPEECH TRANSFORMERS**

3756

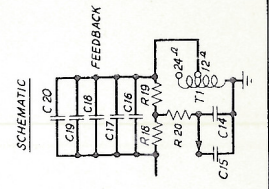
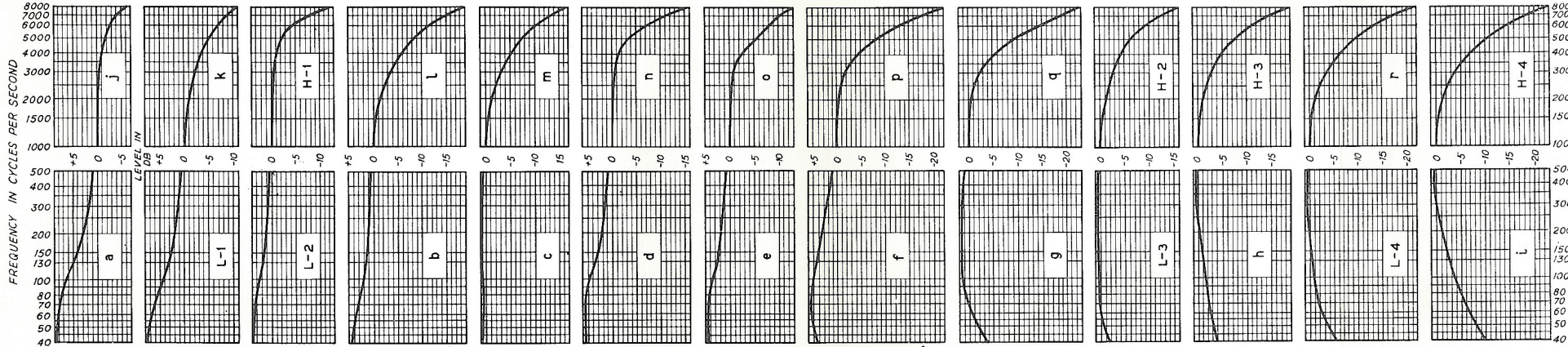
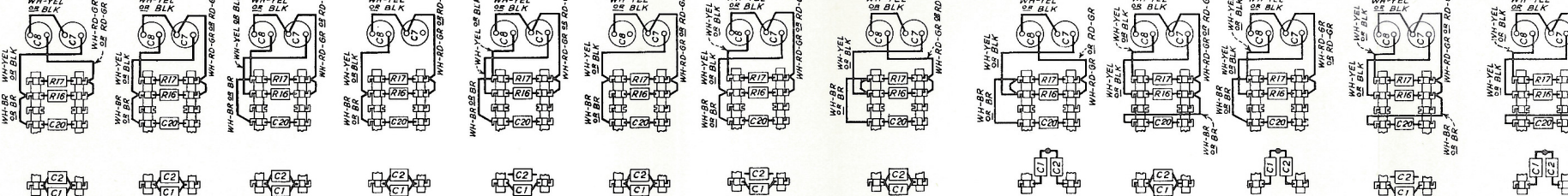


REDRAWN FROM ISSUES WITH FOLLOWING CHANGES: NOTES: 2 AND 4 ADDED. NOTE 3 WAS NOTE 2. AM-1001 AMPLIFIER ADDED TO TITLE, SIMPLEX SOUND SYSTEMS REMOVED. LIMITS  $\pm 1$  DB ADDED IN NOTE 1. WH-YEL OR WH-BL OR WH-RD OR WH-GR ADDED. WH-YEL OR WH-BL OR WH-RD OR WH-GR ADDED TO ALL BLK, BR AND RD-GR WIRES RESPECTIVELY. CURVE DATA REVISED. CURVES CHANGED TO AGREE.  
CFA F&A  
ISSUE: 3 7-22-47

HIGH END WARPING CIRCUIT  
(SEE NOTE 2)  
WIRING DIAGRAM



LOW END WARPING CIRCUIT  
(SEE NOTE 2)  
WIRING DIAGRAM

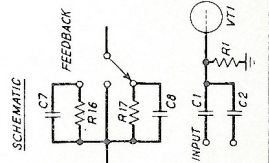


CURVE DATA -- CYCLES & DEVIATIONS FROM REFERENCE IN DB

CURVE DESIGN.	LOW END						HIGH END							
	40	50	60	70	80	90	1000	2000	3000	4000	5000	6000	7000	8000
a	0	0	0	0	0	0	0	0	0	0	0	0	0	0
b	0	0	0	0	0	0	0	0	0	0	0	0	0	0
c	0	0	0	0	0	0	0	0	0	0	0	0	0	0
d	0	0	0	0	0	0	0	0	0	0	0	0	0	0
e	0	0	0	0	0	0	0	0	0	0	0	0	0	0
f	0	0	0	0	0	0	0	0	0	0	0	0	0	0
g	0	0	0	0	0	0	0	0	0	0	0	0	0	0
h	0	0	0	0	0	0	0	0	0	0	0	0	0	0
i	0	0	0	0	0	0	0	0	0	0	0	0	0	0
j	0	0	0	0	0	0	0	0	0	0	0	0	0	0
k	0	0	0	0	0	0	0	0	0	0	0	0	0	0
l	0	0	0	0	0	0	0	0	0	0	0	0	0	0
m	0	0	0	0	0	0	0	0	0	0	0	0	0	0
n	0	0	0	0	0	0	0	0	0	0	0	0	0	0
o	0	0	0	0	0	0	0	0	0	0	0	0	0	0
p	0	0	0	0	0	0	0	0	0	0	0	0	0	0
q	0	0	0	0	0	0	0	0	0	0	0	0	0	0
r	0	0	0	0	0	0	0	0	0	0	0	0	0	0
s	0	0	0	0	0	0	0	0	0	0	0	0	0	0
t	0	0	0	0	0	0	0	0	0	0	0	0	0	0

FOR ADDITIONAL 10' EW-633 OR 8' BELDEN #8401  
ADD 0 -0.1 -0.2 -0.4 -0.6 -0.7

1. THE FREQUENCY RESPONSE CHARACTERISTIC CURVES SHOWN (LIMITS  $\pm 1$  DB) ARE OBTAINED BY ADJUSTMENT OF THE WARPING CIRCUIT IN THE AM-1001 AMPLIFIER (SEE DRAWING WD-113). CURVES L-1 TO L-4 AND H-1 TO H-4 ARE STANDARD. OTHER CURVES ARE FOR USE ONLY WHEN UNUSUAL ACOUSTIC CONDITIONS ARE ENCOUNTERED. ANY LOW END CURVE MAY BE ASSOCIATED WITH ANY HIGH END CURVE.
2. THE CURVES INCLUDE SCANNING LOSS, AND WERE OBTAINED USING ED-35 TEST FILM, 6 FEET OF 3H-2100 COAXIAL CABLE (CAPACITY 8 MMF PER FOOT), AM-101 TYPE VOLUME CONTROL AMPLIFIER AND 15 FEET BELDEN # 8401 MICROPHONE CABLE, CAPACITY 26 MMF PER FOOT. (20 FEET EW-633 PLASTIC MICROPHONE CABLE OPTIONAL).
3. THE FIGURE, ASSOCIATED WITH EACH CURVE, SHOWS THE WARPING CIRCUIT STRAPPING REQUIRED TO OBTAIN THE CURVE. RECONNECT STRAPS, AS NECESSARY, AND REMOVE OTHER EXISTING STRAPS NOT SHOWN IN THE FIGURE. THE WH-BL OR BL AND WH-YEL OR BLK WIRES FROM T1 AND THE WH-RD-GR OR RD-GR WIRES FROM T1 SHOULD REMAIN CONNECTED TO R18, C14 AND R16 RESPECTIVELY AS SHOWN ON DRAWING WD-113.
4. THE AMPLIFIER IS SHIPPED STRAPPED FOR THE L-2, H-2 CURVE.





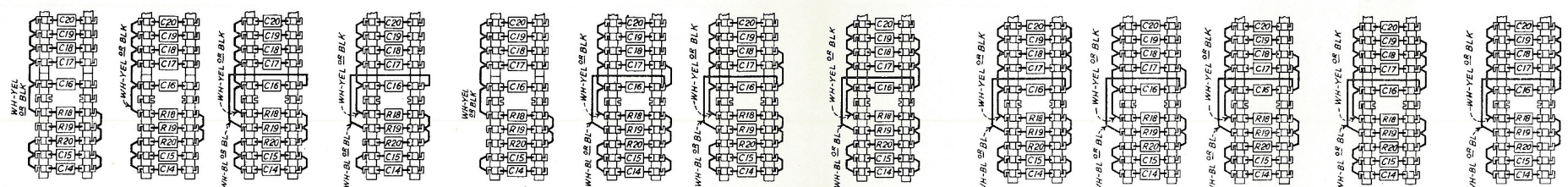




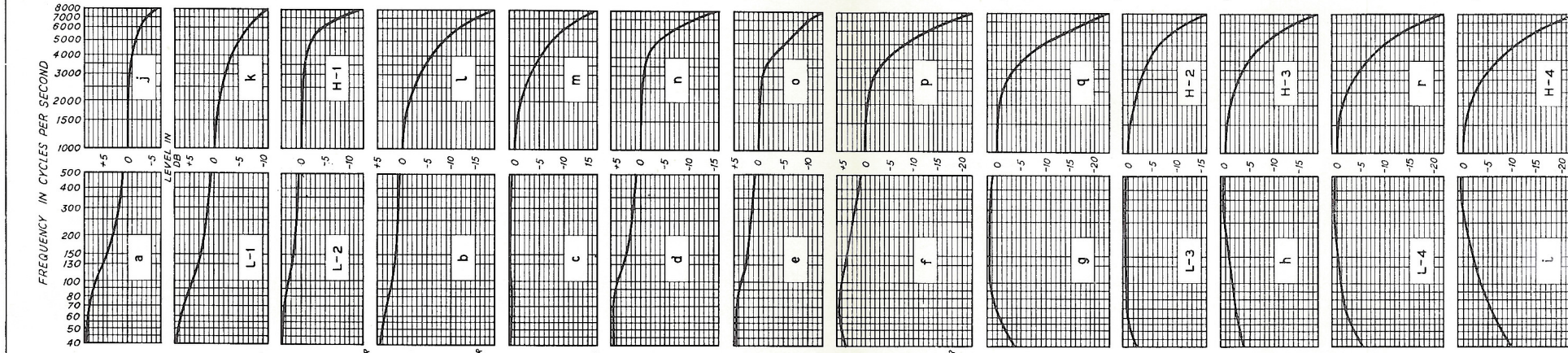
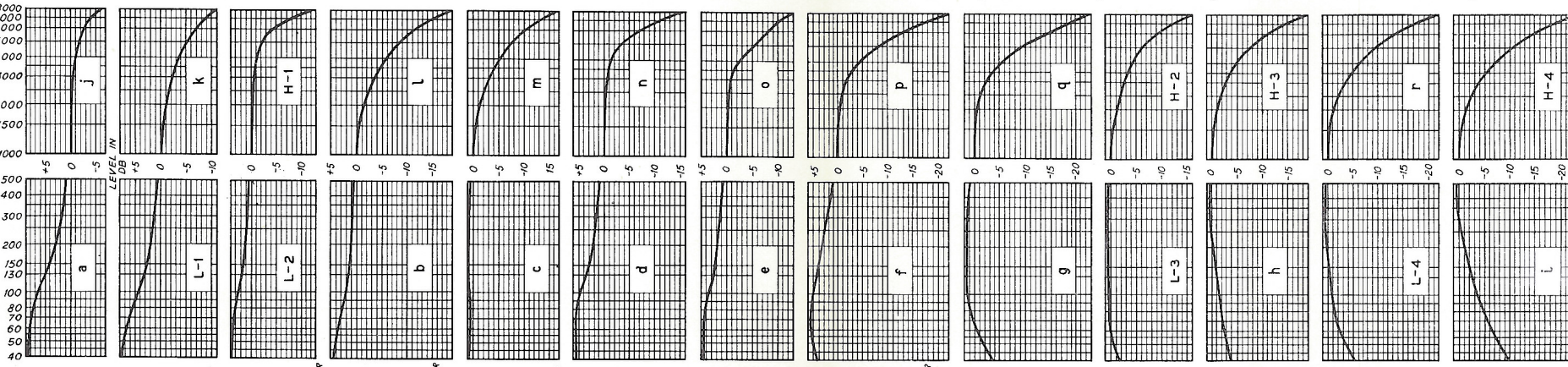
PROGRAM FROM ISSUES WITH FOLLOWING CHANGES: NOTES 3 AND 4 ADDED. NOTE 3 WAS NOTE 2. AM-101 AMPLIFIER ADDED TO TITLE. SIMILAR SOUND SYSTEMS REMOVED. LIMITS  $\pm 1.0$  DB ADDED IN NOTE 1. WH-YEL OR WH-RD OR WH-BL OR WH-GR ADDED. WH-YEL OR WH-BL OR WH-RD OR WH-GR ADDED TO ALL BL, BK, BR AND RD-GR WIRES RESPECTIVELY. CURVE DATA REVISED. CURVES CHANGED TO AGREE.

C.F. 1-6  
ISSUE: 3  
7-22-44

HIGH END WARPING CIRCUIT  
(SEE NOTE 2)  
WIRING DIAGRAM



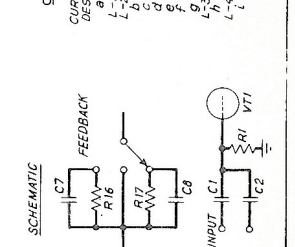
LOW END WARPING CIRCUIT  
(SEE NOTE 2)  
WIRING DIAGRAM



CURVE DATA - CYCLES & DEVIATIONS FROM REFERENCE IN DB

CURVE DESIG.	LOW END				HIGH END					
	40	70	130	500	1000	2000	3000	5000	7000	8000
a	0.6	7.9	4.9	1.9	0	-0.4	-0.7	-1.9	-4.1	-6.1
b	3.9	3.9	3.9	0.6	0	-0.5	-0.5	-0.5	-0.5	-0.5
L-1	4.6	3.0	1.3	0.8	0	-1.5	-3.4	-6.4	-14.9	-16.5
c	0.7	0.7	0.9	0.8	0	-0.4	-0.4	-0.4	-0.4	-0.4
d	4.5	4.3	2.5	1.2	0	-0.3	-0.9	-0.6	-1.0	-13.0
e	4.2	5.5	4.3	2.3	0	-0.5	-1.6	-0.2	-1.4	-22.0
f	-1.9	0.7	0.2	0.3	0	-0.2	-0.3	-0.2	-1.6	-22.9
L-3	-4.0	-2.1	-1.2	0.5	0	-1.2	-3.4	-5.3	-14.6	-16.7
L-4	-10.0	-3.5	-2.6	0	0	-1.2	-3.5	-10.3	-16.5	-22.9
L				0.2	0	-0.1	-0.2	-0.4	-0.6	-0.7

FOR ADDITIONAL INFORMATION SEE BULDEN # 8401



- NOTES
1. THE FREQUENCY RESPONSE CHARACTERISTIC CURVES SHOWN (LIMITS  $\pm 1.0$  DB) ARE OBTAINED BY ADJUSTMENT OF THE WARPING CIRCUIT IN THE AM-101 AMPLIFIER (SEE DRAWING WD-113). CURVES L-1 TO L-4 AND H-1 TO H-4 ARE STANDARD. OTHER CURVES ARE FOR USE ONLY WHEN UNUSUAL ACOUSTIC CONDITIONS ARE ENCOUNTERED. ANY LOW END CURVE MAY BE ASSOCIATED WITH ANY HIGH END CURVE.
  2. THE CURVES INCLUDE SCANNING LOSS, AND WERE OBTAINED USING ED-35 TEST FILM, 6 FEET OF SH-2100 COAXIAL CABLE (CAPACITY 8 MMF PER FOOT), AM-101 TYPE VOLUME CONTROL AMPLIFIER AND 15 FEET BELDEN # 8401 MICROPHONE CABLE, CAPACITY 26 MMF PER FOOT, (20 FEET EW-633 PLASTIC MICROPHONE CABLE OPTIONAL).
  3. THE FIGURE, ASSOCIATED WITH EACH CURVE, SHOWS THE WARPING CIRCUIT STRAPPING REQUIRED TO OBTAIN THE CHARACTERISTICS. RECONNECT STRAPS, AS NECESSARY, AND REMOVE OTHER EXISTING STRAPS NOT SHOWN IN THE FIGURE. THE WH-BL OR BLK AND WH-YEL OR BLK WIRES FROM T1 AND THE WH-RD-GR OR RD-GR WIRE FROM T51 SHOULD REMAIN CONNECTED TO R19, C14 AND R16 RESPECTIVELY AS SHOWN ON DRAWING WD-113.
  4. THE AMPLIFIER IS SHIPPED STRAPPED FOR THE L-2, H-2 CURVE.





## ALTEC LANSING TRANSFORMERS - MATCHING

TYPE	APPLICATION	BALANCED TO GROUND	IMPEDANCES						FREQ- UENCY RANGE	RESPONSE +	MAX. LEVEL REF. 6 db.	SHIELD- ING	OVERALL DIMENSIONS AS MOUNTED (INCHES)	MOUNTING DIMENSIONS (INCHES)
			INPUT			OUTPUT								
			OHMS	CONNECT TO	STRAP	OHMS	CONNECT TO	STRAP						
TJ-403A	HIGH LEVEL AUTO- TRANSFORMER	NO	3 12	WH-BR WH-RD					40- 15000	1 DB	+42.2 DB 100 WATTS	NONE	4 x 4 $\frac{5}{8}$ x 3 $\frac{1}{4}$ H	3 $\frac{1}{2}$ x 4
TL-254C	MEDIUM LEVEL	NO	1000 500 250	1-4 1-3 1-2		12 6	5-7 5-6		20- 20000	1 DB	+35 DB 19 WATTS	NONE	3 $\frac{1}{2}$ x 3 $\frac{3}{8}$ x 4 $\frac{1}{8}$ H	2 $\frac{7}{8}$ x 2 $\frac{3}{8}$
TL-262	MEDIUM LEVEL	NO	250 500 1000	1-2 1-3 1-4		10 20	5-6 5-7		20- 20000	1 DB	+35 DB 19 WATTS	NONE	3 $\frac{1}{2}$ x 3 $\frac{3}{8}$ x 4 $\frac{1}{8}$ H	2 $\frac{7}{8}$ x 2 $\frac{3}{8}$
TP-255A	HYBRID 3 WINDING	YES ALL WINDINGS	500 500	1-2 3-4	2-3 2-3	500	5-14 7-12		20- 10000	1 DB	+15 DB 0.2 WATTS	30 DB	2 $\frac{7}{8}$ x 2 $\frac{1}{2}$ x 3 $\frac{1}{2}$ H	2 $\frac{1}{2}$ x 2
	MATCHING LOW LEVEL	"	1000 250	1-4 1-4	2-3 1-3,2-4	500 125	3-14 3-4	7-12 5-12,7-14	20- 20000	2 DB	"	"	"	"
TP-256	LOW LEVEL	YES	500/600 250/300 125/150 62.5/75	1-6 2-5 1-6 2-5	3-4 3-4 1-4,3-6 2-4,3-5	500/600 250/300 125/150 62.5/75	7-12 8-11 7-12 8-11	9-10 9-10 7-10,9-12 8-10,9-11	20- 20,000	1 DB	+15 DB 0.2 WATTS	40 DB	2 $\frac{7}{8}$ x 2 $\frac{1}{2}$ x 3 $\frac{1}{2}$ H	2 $\frac{1}{2}$ x 2
TP-404	MEDIUM LEVEL AUTO- TRANSFORMER	NO	2.5 5 12	WH-YEL WH-RD WH-BR					50- 8000	1 DB	+35.2 DB 20 WATTS	NONE	2 $\frac{7}{8}$ x 2 $\frac{1}{2}$ x 3 $\frac{1}{2}$ H	2 $\frac{1}{2}$ x 2
TP-258	LOW LEVEL	YES	500/600 250/300 125/150 62.5/75	1-6 2-5 1-6 2-5	3-4 3-4 1-4,3-6 2-4,3-5	500/600 250/300 125/150 62.5/75	7-12 8-11 7-12 8-11	9-10 9-10 7-10,9-12 8-10,9-11	20- 20,000	1 DB	+15 DB 0.19 WATTS	60 DB	2 $\frac{7}{8}$ x 2 $\frac{1}{2}$ x 3 $\frac{1}{2}$ H	2 $\frac{1}{2}$ x 2
TP-261	MEDIUM LEVEL	NO	500	1-2		10 0.5 0.25	3-7 4-7 3-7	5-6 5-6 3-6,5-7	60- 9,000	1 DB	32 DB 10 WATTS	NONE	2 $\frac{1}{2}$ x 2 $\frac{1}{8}$ x 3 $\frac{1}{2}$ H	2 x 2 $\frac{1}{2}$

NOTE: 1, TJ-403A AUTO-TRANSFORMERS ARE RECOMMENDED FOR USE AS FOLLOWS - VOICE OF THE THEATRE SPEAKER SYSTEMS WITH SIMPLEX C60 SOUND SYSTEMS OR EQUIVALENT.

ISSUE	APPROV	DATE	CHANGE	DR BY	APPROV
1		7/15/54		EMC	
2 A		11/15/54	OVERALL WAS OUTSIDE		
2 B		11/15/54	REVISED TO INCLUDE CURRENT ITEMS		
2 C		9/30/58	TP-258 ADDED NOTE CORRECTED.		
			TP-261 ADDED.		

ALTEC LANSING CORPORATION  
MOLLYWOOD, CALIFORNIAMATCHING  
TRANSFORMERS

3754







## ALTEC LANSING POLAR TRANSFORMERS

TYPE	FREQUENCY	PRIMARY TERMINALS	PRIMARY VOLTS	SECONDARY TERMINALS	SECONDARY VOLTS	AMPS.	ELECTROSTATIC SHIELD	OVERALL DIMENSIONS AS MOUNTED ( INCHES )	MOUNTING DIMENSIONS ( INCHES )
TJ-604 B	50-60	1-2 1-3 1-4	105 117 130	5-6-7 8-9-10 11-12	350-0-350 6.3 CT. 5.0	0.125 DC 5.0 3.0	YES	4 x 4 1/2 x 5 1/4 H	3 1/2 x 4
TJ-618 D	50-60	1-2 1-3 1-4	105 117 130	10-12-14 11-12-13 5-6-7 8-9	605-0-605 565-0-565 6.3 CT. 5.0	0.150 DC 3.5 3.0	NO	4 x 4 5/8 x 5 1/4 H	3 1/2 x 4
TJ-619 C	50-60	1-2 1-3 1-4	105 117 130	5-6-7 8-9-10 11-12 13-14 15-16	545-0-545 6.3 CT. 5.0 6.3 6.3	0.200 DC 3.0 3.0 3.0 0.7	NO	4 x 4 3/8 x 5 1/4 H	3 1/2 x 4
TJB-702 (WE-A 3598)	50-60	1-2 1-3	110 120	4-5 7-8-9 6-8-9	5.0 70-0-70 78-0-78	5.0 1.4 1.4	NO	5 1/2 x 4 1/2 x 4 1/2 H	5 x 2 3/4
TL-608	50-60	BLK-BLK	117	RD-RD-TR-RD GR.SLVG-GR- GR.SLVG. 6.3 CT. YEL.SLVG-YEL.SLVG. 5.0	350-0-350 6.3 CT. 5.0	0.125 DC 2.4 3.0	YES	5 1/2 x 3 3/8 x 4 1/8 H	2 7/8 x 2 7/8
TL-706	60	1-2	115	3-4 3-5 3-6	13.0 15.0 17.0	5.0 5.0 5.0	NO	5 1/2 x 3 3/8 x 4 1/8 H	2 7/8 x 2 7/8
TM-602 (WE-A 303B)	50-60	1-2	110	3-3T-4	430-0-430	0.083 DC	NO	3 1/2 x 3 3/8 x 3 1/2 H	2 1/2 x 2 7/8
TMJ-551 (WE-352 Y)	50-60	1-2 1-3 1-3A	105 117 130	4-8-8 7-8-9 10-11	10.0 CT. 10.0 CT. 2.5	3.0 3.0 10.0	NO	5 1/2 x 3 3/8 x 5 H	5 x 2 3/4
TMJ-613	60	1-2	115	3-4-5 6-7-8 9-10-11 12-13-14	440-0-440 6.3 CT. 5.0 CT. 6.3 CT.	0.125 DC 3.0 3.0 2.0	NO	5 1/2 x 3 3/8 x 5 H	5 x 2 3/4
TMJ-701 (UTC-18244)	50-60	1-2 1-3 1-4	107 115 122.5	5-6-7 8-9-10	4.0 CT. 62.5-0-62.5	12.0 2.0 DC	NO		
TML-557	60	1-2	115	3-4 5-6	6.3 6.3	6.0 1.2	YES	4 7/8 x 3 3/8 x 4 1/2 H	3 5/8 x 3 1/8
TML-558	60	1-2	115	3-4-5 6-7-8	6.3 CT. 6.3 CT.	4.2 2.7	NO	4 7/8 x 3 3/8 x 4 1/2 H	3 5/8 x 3 1/8
TMP-550	60	1-2	115	3-4-5	6.3 CT.	4.0	NO	2 3/8 x 2 7/8 x 3 1/2 H	2 x 2 1/2
TMP-551	60	1-2	115	3-4-5 6-7-8	6.3 CT. 6.3 CT.	3.3 0.6	NO	2 3/8 x 2 7/8 x 3 1/2 H	2 x 2 1/2
TMP-590	60	1-2	115	3-4-5 6-7-8	300 CT. 300 CT.	0.010 0.010	NO	2 3/8 x 2 7/8 x 3 1/2 H	2 x 2 1/2
TMP-612	60	1-2	115	3-4 5-6	700 2.5	0.002 3.0	NO	2 3/8 x 2 7/8 x 3 1/2 H	2 x 2 1/2
TMS-578 C (WE-D 96835)	50-60	1-2 1-3 1-4	107 117 130	5-7-9 6-7-8	1725-0-1725 1470-0-1470	0.160 DC 0.160 DC	NO	7 3/8 x 5 1/2 x 7 1/2 H	6 7/8 x 4
TP-701	50-60	1-2 1-3	110 120	4-5	20.0	0.5	NO	2 7/8 x 2 1/2 x 3 1/2 H	2 1/2 x 2
TR-576 A (WE-AQ 1099) (WE-AR 1054A)	50-65	1-2 1-3 1-4	107.5 115 122.5	5-6-7	960-0-960	0.173	NO	8 1/2 x 4 3/8 x 6 H	7 3/8 x 3 1/8
TMS-579 B	50-60	1-2 1-3	110 120	4-5-6	1700-0-1700	0.3	YES	5 1/2 x 7 3/8 x 7 1/2 H	6 7/8 x 4
TM-608 (WE-A 359 A)	50-60	1-2 1-3	110 120	4-5-6 7-8 9-10-11 12-13-14	5-0-5 5.0 492.5-0-492.5 2.5-0-2.5	1.2 2.0 0.130 5.4	NO	4 5/16 x 5 1/2 x 4 1/2 H	5 x 2 3/4
TL-403 AUTO-TRANS. FOR USE WITH A-255 AMPL. ON 220V AC	50-60	0-220	220	0-110	110		NO	3 1/2 x 3 3/8 x 4 1/8 H	2 7/8 x 2 7/8

PRINTED IN U.S.A.

ISSUE	APPROV	DATE	CHANGE	DR BY	APPROV
1		7/1/54			
2		5-22-54	OVERALL WAS 2 7/8		
2-A			NOTES E, F, G ADDED		
2-B		3-27-56	REVISED TO INCLUDE CURRENT ITEMS		
2-C		5-23-56	TMS-579B WAS TMS-579 A		
2-D		5-24-56	TL-403 ADDED		

ALTEC LANSING CORPORATION  
HOLLYWOOD, CALIFORNIA

**POWER  
TRANSFORMERS  
3757**

ALTEC SERVICE CORPORATION

CHOKE COILS, GENERAL

ALTEC LANSING CHOKE COILS

TYPE	APPLICATION	INDUCTANCE			D.C. RESISTANCE OHMS	OVERALL DIMENSIONS AS MOUNTED (INCHES)	MOUNTING DIMENSIONS (INCHES)	
		HENRIES	D.C. M.A.					
TA-305 S	10V 60 CYCLE AC	CONN. TO, STRAP			800 TOTAL	1 3/4 x 1 3/8 DIA.	1 1/2	
		1	1-2	0				
		2	1-3	0				
		3	1-4	0				
		4	1-5	0				
5	1-6	0						
TA-325	10V 60 CYCLE AC	4		0	720	1 3/4 x 1 3/8 DIA.	1	
TBB-301	PLATE FEEDER WITH TP202 & TP204 TRANS.	100	1-4	2-3	5	4600	2 1/4 x 2 3/8 x 2 7/8 H	1 7/16 x 1 7/16
		25	1-4	1-3, 2-4	10	1150		
TBB-314	FILTER	35+			40	500	2 1/4 x 2 3/8 x 2 7/8 H	1 7/16 x 1 7/16
TL-502 A	FILTER	3.5			400	55	3 1/2 x 3 5/8 x 4 1/8 H	2 7/8 x 2 7/8
TL-517 A	FILTER	12			200	126	3 1/2 x 3 5/8 x 4 1/8 H	2 7/8 x 2 7/8
TL-518	FILTER	0.02			5000	0.32	3 1/2 x 3 5/8 x 4 1/8 H	2 7/8 x 2 7/8
TM-504 (WE-179 A)	FILTER	250			5	4317	3 x 3 x 3 3/8 H	2 3/8 x 2 3/8
		200			10			
		175			15			
TM-507	FILTER	8			400	60	4 9/16 x 7 5/8 x 6 H	3 x 7 1/4
		18			100			
TMJ-507 (WE-240 B)	FILTER	25			160	250	4 9/32 x 5 1/2 x 4 7/8 H	5 x 2 3/4
TP-506 B	FILTER	9			150	170	2 7/8 x 2 1/2 x 3 1/2 H	2 1/2 x 2
TP-507	FILTER	3.0			120	60	2 7/8 x 2 1/2 x 3 1/2 H	2 1/2 x 2
TLB-506 A (WE-197 A)	FILTER	15			150	208	5 3/8 x 5 3/8 x 4 3/8 H	3 1/16 x 2 3/16

ISSUE	APPROV.	DATE	CHANGE	DR. BY: E.A.	APPROV. G.H.
1		7/14/51			
2		6-22-52	REVISIONS TO SPECIFICATIONS		
2 A			TL 517 ADDED & TL 502-A		
2 B		11-1-54	REVISED TO INCLUDE CURRENT ITEMS.		
2 C		5-21-56	TP-507 ADDED		
2 D		7-2-56	TLB-506 ADDED		

ALTEC LANSING CORPORATION  
HOLLYWOOD, CALIFORNIA

CHOKES

3755





\* Indicates Additions and Changes.

Replaces Transformers - Power, Section  
 of E.B. "Transformers - General", File 4.4g

TRANSFORMER	WHERE USED	* FREQ.	* PRIMARY		* SECONDARY			* REMARKS
			WINDINGS	VOLTS	WINDINGS	VOLTS	AMPS.	
90-B Repeating Coil	Filament & Plate 25-C & 51-A Amplifiers	60	1-2	105-115	3-4, 5-6 7-8 9-10	5.0 5.0 390.0	1.6 1.6 0.030	4, 5 are Center Taps for Winding 3-6, 8 & 9 are Strapped
303-A Transformer	Filament & Plate 34-A & 34-B Amplifiers	60	1-2	110	3-4 5-6 7-8 8-9	1.0 4.5 4.5 385.0	0.25 1.6 1.6 0.030	"T" is Common Center Tap for Windings, 3-4 & 5-6
303-B Transformer	Plate, 42-A, 46-A, B, C, D, E & F Amplifiers	60	1-2	110	3-3T 3T-4	430 430	0.063 0.063	
303-C Transformer	Filament, 42-A, 46-A, B, C, D, E & F Amplifiers	60	1-2	110	3-3T-4 5-5T-6	4.5 4.5	3.2 3.2	3T & 5T are Center Taps
303-D Transformer	Plate, 706-A Control Cabinet	720	1-2A-2B	90	3-4 5-5T-6			Supplies Plate Potential for 2, 205-D Tubes in Full Wave Rect. 1, 205-D Tube in Half Wave Rect. "5T" is Center Tap for 5-6
303-F Transformer	Filament, TA-7114 Panel	50-60	1-2 1-3 1-4	107.5 115.0 122.5	5-7 8-10	4.5 4.5	3.2 3.2	6 & 9 are Center Taps for Windings, 5-7 & 8-10
307-A Transformer	Plate, 43-A Amplifier	60	1-2	110	3-3T 3T-4	760 760	0.13 0.13	
307-B Transformer	Filament, 43-A & B-43-A Amplifiers	60	1-2	110	3-3T-4 5-5T-6	10.0 10.0	6.0 6.0	3T & 5T are Center Taps
308-A Transformer	707-A Control Cabinet	60	1-2 3-4	110 110	5-6 5-6	5.0 10.0	16.0 16.0	Line Voltage Regulator
310-A Transformer	Filament & Plate, 708-A Control Cabinet	60	1-2 1-3 1-4	105.0 110.0 115.0	5-7 6-7 8-9 10-11 12-13	450 450 300 4.65 4.65	0.080 0.080 0.043 3.2 3.2	Half Wave Rectifier
311-A Transformer	Projection Lamp, 202-B & TA-4050 -53 Reproducer Sets	-	-	-	-	-	-	Replaced by 311-B Trans- former
311-B Transformer	Projection Lamp, 202-B & TA-4050 -53 Reproducer Sets	60	1-2	100-125	3-4	30	30	8 Taps on Primary to Adjust for Line Voltage
316-A Transformer	Plate, 57-A, 59-A & 59-B Amplifiers	50-60	1-2 1-3 1-4	107.5 115.0 122.5	5-6 7-8	655 655	0.130 0.130	Full Wave Rectifier
*316-B Transformer	5-A Rectifier	50-60	1-2 1-3 1-4	107.5 115.0 122.5	5-6-7 8-9-10	5.0 720	2.0 0.125	6 & 9 are Center Taps. Full Wave Rectifier.
317-A Transformer	Filament, 57-A Amplifiers	50-60	1-2 1-3 1-4	107.5 115.0 122.5	5-6 7-9 10-12 13-15	2.52 2.2 5.0 5.0	6.0 3.0 2.0 2.0	8, 11 & 14 are Center Taps for Windings, 7-9, 10-12 & 13-15





\* Indicates Additions & Changes \*

TRANSFORMER	WHERE USED	FREQ.	PRIMARY		SECONDARY			REMARKS
			WINDINGS	VOLTS	WINDINGS	VOLTS	AMPS.	
317-C Transformer	Filament, 59-A & 59-B Amplifiers	50-60	1-2 1-3 1-4	107.5 115.0 122.5	5-6 7-8-9 10-11-12 13-14-15	2.52 10.0 5.0 5.0	6.0 0.70 2.0 2.0	8, 11 & 14 are Center Taps for Windings, 7-9, 10-12 & 13-15
319-A Transformer	Filament, 10-A Radio Receiver	50-60	1-2 1-3 1-4	107.5 115.0 122.5	5-6-7	2.13	8.0	6 is Center Tap, for Winding 5-7
321-A Transformer	Filament, 63-A Amplifier	50-60	1-2 1-3 1-4	107.5 115.0 122.5	5-6-7	10.0	0.70	6 is Center Tap, for Winding 5-7
322-A Transformer	10 Volt Supply, D-94852 & D-94852-B & D Control Unit	50-60	1-2	100	3-4	11.5	0.70	
325-A Transformer	Filament, 5-A Current Supply Set	50-60	1-2 1-3 1-4	107.5 115.0 122.5	5-7 8-10	2.5 2.5	16.0 16.0	6 & 9 are Center Taps
326-A Transformer	Plate, 5-A Current Supply Set	50-60	10)-3 9)-2 8)-1 7) 6) 5) 4)	107.5 115.0 122.5	11-12-13 14-15-16	40-64 40-64	3.0 3.0	12 & 15 are Center Taps. Taps 10,9,8,7,6,5 & 4 are used to adjust the secondary voltage.
327-A Transformer	Filament & Plate, D-94531 & D-95036 type Amplifiers except D-95036-E	50-65	1-2 1-3 1-4	107.5 115.0 122.5	5-7 8-10 11-13 14-16	5.0 10.0 5.0 834.0	2.5 0.7 2.0 0.108	6, 9, 12 & 15 are Center Taps for Windings, 5-7, 8-10, 11-13 & 14-16
328-A Transformer	Projector Lamp, D-94644 Type, Reproducer Set	60	4-7 3-7 2-7 1-7	100.0 107.5 115.0 122.5	5-6	20.0	12.5	5-6 is part of Winding, 1-7
*332-B Transformer	Filament & Plate, 86-A type Amplifiers	60	1-2 1-3	110 120	4-6 7-9 10-12 13-14	5.0 10.0 1120.0 5.0	2.4 1.92 0.106 2.0	Terminals 5, 8 & 11 are Center Taps for Windings, 4-6, 7-9 & 10-12
*352-A Transformer	Filament & Plate, 91-A Amplifier	60-63	1-2 1-3	110 120	4-6 7-8 9-11 12-14	10.0 5.0 1000.0 5.0	0.64 2.0 0.130 1.2	5, 10 & 13 are Center Taps for Windings 4-6, 9-11 & 12-14
*352-B Transformer	12-A Rectifier	60-63	1-2 1-3	110 120	4-5 6-8	5.0 130.0	6.0 1.4	7 is Center Tap for Winding 6-8
*357-A Transformer	Filament & Plate, 86-B & 86-C Amplifiers	50-60	1-2 or 1-3	110-120 110-120	4-6 7-9 10-12 13-14	5.0 10.0 1120.0 5.0	2.4 1.92 0.106 2.0	Terminals 5, 8 & 11 are Center Taps for Windings 4-6, 7-9 & 10-12
*359-A Transformer	Filament & Plate, 91-B Amplifier	50-60	1-2 or 1-3	110-120 110-120	4-6 7-8 9-11 12-14	10.0 5.0 985.0 5.0	1.2 2.0 0.130 2.4	Terminals 5, 10 & 13 are Center Taps for Windings 4-6, 9-11 & 12-14
*359-B Transformer	12-B Rectifier	50-60	1-2 or 1-3	110-120 110-120	4-6 7-9 10-12	5.0 10.0 1120.0	2.4 1.92 0.106	Terminals 5, 8 & 11 are Center Taps for Windings 4-6, 7-9 & 10-12
*ASL-2852 Transformer	Filament & Plate, TA-7321 Power Unit		1-2	115	C-17 C-18 C-19 C-20	17.0 18.0 19.0 20.0		



TRANSFORMER	WHERE USED	FREQ.	PRIMARY		SECONDARY		AMPS.	REMARKS
			WINDINGS	VOLTS	WINDINGS	VOLTS		
D-87299 Transformer (Now Coded, 310-A)	Filament & Plate, 708-A Control Cabinet	60	1-2	105	5-6	450	0.08	
			1-3	110	6-7	450	0.08	
			1-4	115	8-9	300	0.043	
					10-11	4.65	3.2	
				11-12	4.65	3.2		
D-88444 Transformer	Plate, D-88446 Amplifier	25-60	1-2	110	3-3T 3T-4	430 430	0.063 0.063	This rating is for 25 Cycles
D-88445 Transformer	Filament, D-88446 Amplifier	25-60	1-2	107.5	3-4	4.5	3.2	
			1-3	115.0	5-6	4.5	3.2	
			1-4	122.5				
D-95557 Transformer	Plate, B-43-A, Amplifier	50-65	1-2	107.5	5-7	1920	1.73	6 is Center Tap of Winding 5-7
			1-3	115.0				
			1-4	122.5				
D-95660 Transformer	Filament, TA-7249 Rectifier	50-65	1-2	107.5	5-7	2.64	14.0	6 is Center Tap for Winding 5-7
			1-3	115.0	8-10	10.0	0.7	
			1-4	122.5	11-13	5.0	2.0	
					13-16	920.0	0.078	
D-95661 Transformer	Plate, TA-7249 Rectifier	50-65	1-2	107.5	5-7	3180	0.198	
			1-3	115.0				
			1-4	122.5				
D-95998 Transformer	Filament & Plate, D-95036-E Amplifier	50-65	1-2	107.5	5-7	5.0	2.5	6, 9, 12 & 15 are Center Taps for Windings 5-7, 8-10, 11-13 and 14-16
			1-3	115.0				
			1-4	122.5				
D-96835 Transformer	Plate, 87-A, B-87-A & 87-C Amplifiers	47-63	1-2	110	4-6	2940	0.121	5 is Center Tap for Winding 4-6
			1-3	120				
D-96836 Transformer	Filament, 87-A, B-87-A & 87-C Amplifiers	47-63	1-2	110	4-6	10.0	3.2	5, 8 & 11 are Center Taps for Windings 4-6, 7-9 and 10-12
			1-3	120	7-9 10-12	10.0 2.59	3.2 30.0	
*D-96970 Transformer	Filament & Plate, 86-C & B, & C-86-A Amplifiers	50-60	1-2	110	4-6	5.0	2.4	5, 8 & 11 are Center Taps for Windings 4-6, 7-9 and 10-12
			1-3	120	7-9	10.0	1.92	
					10-12	1120.0	0.106	
					13-14	5.0	2.0	
KS-2261 Transformer	Filament, 520-A, 521-A and D-94836 Panels	60	1-2	110	5-9	14.0	12.0	7 is Center Tap
			3-4		6-8		10.0	
KS-2264 Transformer	Plate, 520-A & D-94836 Panels	60	1-2 3-4	110 220	5-7	2200	0.7	6 is Center Tap of Winding 5-7
KS-6154 Transformer	Filament & Plate, 700-A Control Cabinet	20	4(start)	90	5-6	5.0	3.2	10 is Center Tap for Winding 9-11
			1	65	7-8	5.0	3.2	
			2	75	9-11	800.0	0.10	
			3	85				
KS-6155 Transformer	Filament & Plate, 701-A Control Cabinet	50-60	1-2	100	9-10	5.0	3.2	19 is Center Tap for Winding 18-20
			1-3	105	11-12	5.0	3.2	
			1-4	110	13-14	5.0	3.2	
			1-5	115	15-16	350	0.06	
			1-6	120	15-17	400	0.06	
			1-7	125	18-20	900	0.06	
			1-8	130				
*T-5797 Transformer	TA-4151 Loud- speaking Telephone	50-60	BL-BL	105-125	-	-	-	See E.B. "Loudspeaking Tele- phones, TA-4151 & TA-4153 Types", File 4.22.
*T-7186 Transformer	TA-4165 Loud- speaking Telephone	50-60	BL-BL	105-125	-	-	-	See E.B. "Loudspeaking Tele- phones, TA-4165 & TA-4166 Types", File 4.22.





\* Indicates Additions & Changes \*

TRANSFORMER	WHERE USED	FREQ.	PRIMARY		SECONDARY			REMARKS
			WINDINGS	VOLTS	WINDINGS	VOLTS	AMPS.	
TA-7278 Transformer	Filament & Plate, TA-7276 Power Unit	50 to 62.5	1-2 1-3 1-4 1-5 1-6 1-7	100 105 110 115 120 125	Coil #1 (Fil.) Coil #2 (Fil.) Coil #1 (Anode) Coil #2 (Anode)	2.25 2.25 33.0 33.0	17.0 17.0 6.0 6.0	
#51157 Transformer (Heyer Products Co.)	Filament & Plate, TA-4144 Power Unit	50 to 62.5	1-2 1-3 1-4 1-5 1-6 1-7	100 105 110 115 120 125				Secondary Supplies Anode and Filament of Two #189048 Tungar Bulbs
#79884 Auto-Transf. (G.E.Co.)	In 220 Volt Out- put of KS-5321 Motor Generator Set	5-140	1-2	220	3-4	110	13.6	Has Flexible Leads Approx. 6" Long
#102311 Transformer (Heyer Products Co.)	Filament & Plate, TA-4038 Power Unit	50 to 62.5	1-2 1-3 1-4 1-5 1-6 1-7	100 105 110 115 120 125				Secondary Supplies Anode and Filament of Two #189048 Tungar Bulbs
#211312 Transformer (Heyer Products Co.)	Filament & Plate, TA-4035 Power Unit	50 to 62.5	1-2 1-3 1-4 1-5 1-6 1-7	100 105 110 115 120 125				Secondary Supplies Anode and Filament of Four #189048 Tungar Bulbs
#325311 Transformer (Heyer Products Co.)	Filament & Plate, TA-4036 Power Unit	50 to 62.5	1-2 1-3 1-4 1-5 1-6 1-7	100 105 110 115 120 125				Secondary Supplies Anode and Filament of Two #189048 Tungar Bulbs
#330304 Transformer (Heyer Products Co.)	Filament & Plate, TA-4033 Power Unit	50 to 62.5	1-2 1-3 1-4 1-5 1-6 1-7	100 105 110 115 120 125				Secondary Supplies Anode and Filament of Two #189048 Tungar Bulbs
#799827 Transformer (W.E. & Mfg. Co.)	KS-7146 type Current Supply Sets	50 to 62.5	1-2 1-3 1-4	105-110 111-119 120-125	5) Aging 6) Steps 7) 2.0 8) Volts 9) Per 10) Step			Secondary Feeds a Rectox Unit which has an output of 2.0 Amps. at 20.0 Volts.



REPLACING OUTPUT TRANSFORMER & REPEATING COIL SECTION OF E.E. TRANSFORMERS - GENERAL, FILE 4,48							
*INDICATES ADDITIONS OR CHANGES.							
TRANSFORMER	USE	IMPED. RATIO (OHMS)	* SHIELD	*AVERAGE DC RESISTANCE (See Note)			
				L. WINDING	*RES.	H. WINDING	*RES.
<b>Output Transformer</b>							
113-A	Output, 9-A Ampl. . . . .	8000:500	E	1-2 & 5-6	20	3-4 & 7-8	317
113-C	Output, 10-A Ampl. . . . .	3000:500	E	1-2 & 5-6	25.2	3-4 & 7-8	228
120-A	Output, 8-B & 17-F Ampls. . . . .	6000:500	No	1-2 & 3-4	104	5-6 . . .	695
120-F	Output, 34-A & 34-B Ampls. . . . .	4000:4000	No	1-2 & 3-4	450	5-6 . . .	450
120-G	Output, 32-A Ampl. . . . .	4000:2000	No	1-2 & 3-4	210	5-6 . . .	450
120-H	Output, 25-C & 51-A Ampls. . . . .	4000:35	No	1-2 & 3-4	4.13	5-6 . . .	565
127-A	Output, 42-A & 46-E Ampls. . . . .	8000:500:250	No	1-2-3-4	58.5	5-6 & 7-8	925
127-C	Output, 49-A, 49-B, 49-C, 50-A, D-85943, D-86729, & TA-7310 type Ampls. and 207-A Panel . . . . .	23000:500	No	1-2 & 5-6	67	3-4 & 7-8	3220
127-D	Output, 46-A,B,C,D,F type & D-88446 Ampls. . . . .	7200:8	No	1-2 . . .	0.675	3-4 & 5-6	860
128-A	Output, 43-A Ampl. . . . .	6500:500	No	1-2 & 5-6	18.2	3-4 & 7-8	200
130-A	Output, 47-A, 47-B, 53-A & 53-B Ampls. . . . .	25000:200	No	1-2 & 3-4	37.2	5-6 . . .	2440
131-A	Output, 8-C Ampl. . . . .	6000:500	No	1-2 & 3-4	105	5-6 . . .	695
132-A	Output, 48-A & 54-A Ampls. . . . .	25000:200	No	1-2 & 3-4	37	5-6 . . .	2440
132-C	Output, 62-A, TA-7246 & TA-7261 Ampls. . . . .	23000:500	No	1-2 & 5-6	56	3-4 & 7-8	2740
134-C	Output, 57-A Ampl. . . . .	6800:500	No	1-2 & 5-6	23	3-4 & 7-8	122
134-D	Output, 59-A & 59-B Ampls. . . . .	6800:500:8	No	1-2-3 . .	21	4-5 & 6-7	177
139-A	Output, 10-A Radio Receiver . . . . .	30000:140	No	1-2 . . .	12	3-4 . . .	3950
144-A	Output, D-94531 & D-95036 type Ampls., except D-95035-E Ampls. . . . .	6800:8	No	1-2 . . .	0.37	3-5 . . .	140
147-A	Output, 63-A Ampl. . . . .	25000:200	No	1-2 & 3-4	38	5-6 . . .	2430
150-A	Output, 80-A & 80-B type Ampls. . . . .	25000:200	No	1-2 & 3-4	38	5-6 . . .	2500
*159-B	Output, 86-C & B-86-A Ampls. . . . .	( 4130:12 ( 4130:6		1-2 . . .	.515	3-4 & 5-6	167
166-A	Output, 86-A type Ampl. . . . .	4130:12:6	No	1-IT-2	0.49	3-4 & 5-6	120
170-A	Output, FEC 209-A & B Repro. Sets and TA-7391 Coupling Unit . . . . .	357000:25	No	1-2 . . .	3.4	3-4 . . .	4400
171-A	Output, 91-A Ampl. . . . .	( 3000:9 ( 1900:3.5 ( 1190		1-3 . . .	.825	4-5-6-7 .	143
D-95659	Output, B-10-A, C-10-A, D-10-A, B-43-A, C-43-A, 87-A & TA-7248 & TA-7248-A Ampls. . . . .	8000:16	No	(5-6 & 7-8 ( & 9-10 & (11-12	0.44	1-2 & 3-4	77.5
D-95995	Output, D-95036-E Ampl. . . . .	6800:16		1-2 & 3-4	0.85	5-7 . . .	178
D-96736	Output, D-46-A, D-46-B, H-46-C & F-46-F Ampls. . . . .	18000:5	No	1-IT-2	0.23	3-4 & 5-6	590
<b>Repeating Coil</b>							
80-A	Radio Broadcasting Systems . . . . .	200:500	No	1-2 & 5-6	13.8	3-4 & 7-8	42.5
80-B	D-88449 type Panels & Radio Broadcasting Systems . . . . .	200:200	No	1-2 & 5-6	18.3	3-4 & 7-8	22.6
105-A	201 type Panels . . . . .	200:50	No	1-2 & 5-6	10	3-4 & 7-8	24
111-C	Output, TA-7294 Control Cabinet . . . . .	600:600	E	1-2-5-6 .	35	3-4-7-8-	35
118-A	Output, 711-A Control Cabinet . . . . .	200:200	No	1-2 & 5-6	12.6	3-4 & 7-8	12.6
D-87744	Output, 711-A type Control Cabinet . . . . .	200:200	No	1-2 & 5-6	12.6	3-4 & 7-8	12.6
(now coded 118-A)							
D-93957	Ant. Coupling, 10-A Radio Receiver (245-B & 246-A Panels) . . . . .	100:1000	E	1-2 & 5-6	0.4	3-4 & 7-8	4
(now coded 137-A)							
D-94288	"Vertical" Input, D-94255 type Control Cabinet & TA-7253 type Equalizer . . . . .	5:500	No	1-2 . . .	0.44	3-4 . . .	41
D-96245	TA-7284 Control Cabinet . . . . .	16:500	No	1-2 . . .	0.33	3-4 . . .	12.5
*D-97823	Music Reproducing Systems . . . . .	5:500	M	1-2 . . .	0.30	3-10 . . .	2800
(now coded 141-A)							

E - Electrostatic Shield; M - Magnetic Shield.  
Note: The "Average" D.C. Resistances are for, (a) the Low windings in series, (b) the High windings in series. These values are for checking purposes only, because of manufacturing limits, to permit the adjustment of turns for inductance unbalance, etc. The "Maximum" or "Minimum" D.C. Resistance may vary 12% from the "Average".









REPLACING INPUT-TRANSFORMER SECTION OF  
E.B. TRANSFORMERS - GENERAL, FILE 4.48  
INPUT TRANSFORMERS

* INDICATES ADDITIONS OR CHANGES.		IMPED. RATIO (OHMS)	* SHIELD	*AVERAGE DC RESISTANCE (See Note)			
TRANSFORMERS	USE			L. WINDING	*RES.	H. WINDING	*RES.
<b>Auto-Transformers</b>							
7-A	TA-7257 Network, 200-A, 209-A, ASL-2828 & D-85125 Panels . . . . .	500:16	No	2-13 . .	-	1-13 . . . .	10.4
*TA-4183	Music Reproducing & P.A. Systems . . . . .	50:8.0:Var.	No	L-C or H-C	-	1-C or 10-C	-
<b>Induction Coil</b>							
#13	521-A Subscriber Set . . . . .	. . . . .	No	F-F . . .	1.3	8-8 . . . . .	16.9
#66	D-85125 Panel . . . . .	. . . . .	No	1-2 . . .	5.6	3-4 . . . . .	79.5
<b>Input Transformers</b>							
208-AD	Input, 518-B Panel . . . . .	500:14000	No	1-2 . . .	54	(3-4-5-6-7- (8-9-10-11- (12-13-14 . . .	3400
208-E	700-A Control Cabinet . . . . .	600:80000	E	1-2 & 5-6	5.8	3-4 & 7-8 . . .	335
208-F	Input, 9-A Ampl. . . . .	4000:70000	No	1-2 & 5-6	895	3-4 & 7-8 . . .	5050
208-W	Input, 10-A Ampl. . . . .	4000:8000	No	1-2 & 5-6	305	3-4 & 7-8 . . .	310
226-B	Interstage, 8-B & A-8-B Ampls. . . . .	6000:165000	No	1-2 . . .	19800	1-4 . . . . .	10500
226-G	Input, 32-A Ampl. . . . .	20000:133000	No	1-2 . . .	2190	3-4 . . . . .	6950
226-H	Input, 34-A & 34-B Ampls. . . . .	200:100000	No	1-2-3 . . .	58	4-5-6-7-8 . . .	6300
227-A	Interstage, 34-A & 34-B Ampls. . . . .	20000:133000	No	1-2 & 3-4	2190	5-6 . . . . .	5650
227-C	Input, 25-C & 51-A Ampls. . . . .	35:140000	No	1-2 . . .	3.8	3-4 . . . . .	6180
233-B	Input, 8-B & A-8-B Ampls. . . . .	200:25000	No	1-2 & 3-4	37.4	6-7-8 . . . . .	2440
233-D	Interstage, 32-A, D-85943, D-85943-A & E, D-86729, D-86729-A & E, and TA-7310 Ampls. . . . .	20000:50000	No	1-2 & 5-6	3020	3-4 & 7-8 . . .	4740
233-E	Input, 32-A, 41-A, A-41-A, 41-B, E-41-C Ampls. (See D-88822 Input Transf.) . . . . .	200:25000	No	1-2 & 5-6	52.2	3-4 & 7-8 . . .	3920
233-F	Input, 203-B Panel . . . . .	500:14000	No	1-2 . . .	143	3-4 . . . . .	3890
233-G	Input, 42-A Ampl. . . . .	16000:64000	No	1-2 & 5-6	2600	3-4 & 7-8 . . .	5200
233-H	Interstage, 46-A, 46-B type & D-88446 Ampls. . . . .	20000:180000	No	1-2 . . .	1740	3-4 & 5-6 . . .	5210
233-J	Input, 46-A, 46-B type & D-88446 Ampls. (Replace with 247-A and Det. 1-A, ASP-930 Mounting Plate) . . . . .	250:250000	No	1-2 & 3-4	70.5	5-6 . . . . .	7600
241-A	Input, A-10-A, C-10-A & 43-A type Ampls. . . . .	275:3370	No	1-2 & 5-6	62	3-4 & 7-8 . . .	895
242-B	706-A & 708-A Control Cabinets . . . . .	600:80000	No	1-2 & 5-6	16.5	3-4 & 7-8 . . .	1680
246-A	Interstage, 49-A, 49-B & 49-C type, D-85943-E, C, & D, D-86729-B, C & D, D-94531-A & D-95036-A & B Ampls. . . . .	13000:117000	No	1-2 & 5-6	1690	3-4 & 7-8 . . .	6000
247-A	Input, 46-C, D, E & F type, D-46-B, A-80-B, D-90500, D-94013, TA-7261 & TA-7246 Ampls. . . . .	250:159000	No	1-2 & 3-4	75	5-6 . . . . .	5740
247-B	Interstage, 46-C, D, E & F type & D-46-B Ampls. . . . .	16000:100000	No	1-2 & 5-6	2050	3-4 & 7-8 . . .	5200
247-H	Input, 59-A Ampl. . . . .	200:135000	No	1-2 & 3-4	15.4	5-6 . . . . .	4850
247-J	Input, 57-A Ampl. . . . .	250:75000	No	1-2 & 5-6	26.8	3-4 & 7-8 . . .	3900
247-Y	Interstage, 59-A & 59-B Ampls. . . . .	16000:75000	No	1-IT-2 . .	1150	3-4 & 5-6 . . .	3400
247-L	Interstage, 59-A & 59-B Ampls. . . . .	17000:113000	No	1-2 . . .	1350	3-4 . . . . .	4300
257-A	Detector Input, 10-A Radio Receiver . . . . .	1:1	No	1-2 . . .	-	3-4 . . . . .	-
258-A	Input, D-94531 & D-95036 type Ampls., except D-95036-E Ampl. . . . .	200:80000	M	Rd-B1 . .	43.5	Gr-B1, Wh. . .	5750
260-A	Interstage, D-94531 & D-95036 type Ampls., except D-95036-E Ampl. . . . .	18000:84000	No	1-2 . . .	2260	3-5 . . . . .	5200
261-A	Input, 59-A, 59-B & 63-A Ampls. (Mid tap for 387 Transmitter) . . . . .	200:135000	M	1-2-3-4 . .	15.2	5-6 . . . . .	4850
261-B	Input, 86-A type Ampls. . . . .	200:110000	E&M	1-2 & 3-4	15.7	5-6 . . . . .	4440
264-A	Input, 80-A Ampl. . . . .	25:150000	M	1-2 & 3-4	0.96	5-6 . . . . .	3990
264-B	Input, 80-B & D-95036-E & F Ampls. . . . .	200:135000	M	1-2 & 3-4	15.4	5-6 . . . . .	4760
264-C	Interstage, 86-A type Ampls. . . . .	18000:100000	No	1-2 . . .	2010	3-4 & 5-6 . . .	4950
*285-A	Input, 91-A Ampl. . . . .	30:200000	E&M	1-2 . . .	5	3-4 . . . . .	4400
D-88822	Spec. Input, 41-A Ampl. for 6 db Increased Gain . . . . .	200:100000	No	1-2 & 5-6	8.6	3-4 & 7-8 . . .	3900
D-95072	Input, 41 & 53 type Ampls. using 618 Transmitter . . . . .	30:150000	No	1-2 & 3-4	2.26	5-6 . . . . .	3900
D-95658	Input, B-10-A, 87-A & TA-7248 & TA-7248-A Ampls. . . . .	250:30900	No	1-2 & 5-6	66	3-4 & 7-8 . . .	4700
D-95997	Interstage, D-95036-E Ampl. . . . .	17000:113000	No	1-2 . . .	1370	3-4 . . . . .	3990

E - Electrostatic Shield; M - Magnetic Shield.  
 Note: The "Average" D.C. Resistances are for, (a) the Low windings in series, (b) the High windings in series. These values are for checking purposes only, because of manufacturing limits, to permit the adjustment of turns for inductance unbalance, etc. The "Maximum" or "Minimum" D.C. Resistance may vary 12% from the "Average".







## 1. DESCRIPTION

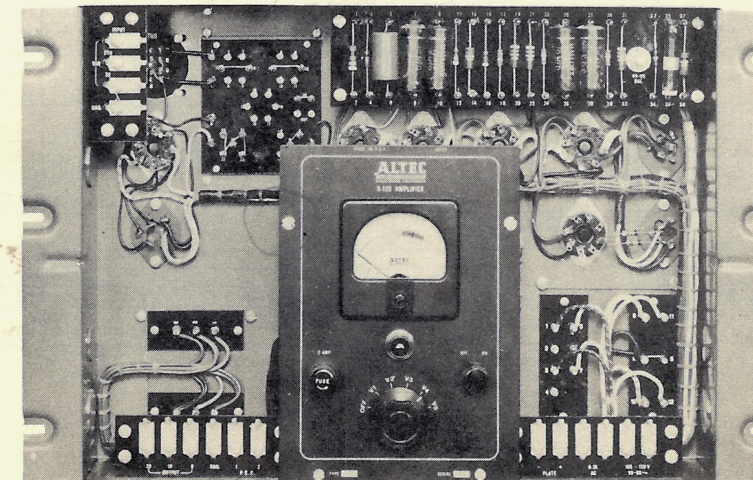
1.1 The A-126 Amplifier is an all AC operated voltage gain and power amplifier, of recessed panel type construction with a removable front panel. The amplifier consists of 2 voltage stages, a phase inverter and a pushpull stage and has provision for tapped attenuation in steps of 4, 8 and 12 db. It is equipped with an equalizer section for HF and LF equalization which is so designed that there is no insertion loss for any setting of equalization. It supplies plate and filament voltage for 2 Altec Lansing A-421 Cathode Follower Amplifiers as well as for pre-amplifiers. A potentiometer is included in the cathode circuit of the output stage to balance tubes for maximum power and minimum hum.

## 2. CHARACTERISTICS

GAIN	90 db Max.
ATTENUATION	Taps for 4, 8 and 12 db attenuation from full gain
POWER OUTPUT at 8% Intermodulation or 2% Total Harmonics	15 watts / 41.8 dbm *
FREQUENCY RESPONSE	Flat within 1 db 20-20,000 cps with Equalizer strapped out
NOISE LEVEL	-27.2 dbm *
IMPEDANCE Input (Source) Output (Load)	30 - 250 - 500 ohms 10 or 20 ohms
VACUUM TUBES	2-6J7; 1-6J5; 2-6L6G; 1-5U4G; 1-0C3 VR
POWER REQUIRED	105/130 volts 50/60 cycles 110 watts
POWER SUPPLIED	85V regulated DC for 2 Altec Lansing A-421 Cathode Follower Amplifiers and PEC'S with 1 milliamp drain. Also 300 V DC at 30 MA - and 6.3 V AC at 2 amp
FUSING	2 Amp. Bus 3 A G
EQUALIZATION	See Correction Data - Page 2
DIMENSIONS	12-1/4" high x 19" long x 9-1/4" deep
WEIGHT	39 lbs.

\* dbm uses a reference level of 1.0 milliwatt (0.001 watt). To correct to reference of 6.0 milliwatts (0.006 watt) subtract algebraically 7.8 db.

ASSOCIATED DRAWING - 3885





## 3. EQUALIZATION

3.1 An equalizer, a simplified circuit of which is shown in the lower left hand corner of Drawing 3885, is incorporated as an integral part of this amplifier which provides a large number of combinations of equalization. Basically, it permits of individual settings of Low End droop, Low End rise, High End cut-off and High End rise.

The low droop section involves equalizer terminals 1,2,3,4,5,6 normal flat 1-4  
 " " rise " " " " " 7,8,9,10,11,12 " " 7-10  
 " high " " " " " 13,14,15,16 " " open 13 and 16  
 " " cut-off " " " " " In,Out,13,20,21,22 " " Out,(no strap on "In")

A combination of the various strappings listed in the correction chart will provide practically any equalization curve desired for a given condition.

The equalizer consists of 4 individual equalizer sections any one of which may be employed separately or combinations of any 2 or more sections can be used collectively. For example, a combination of low droop classification 11, low rise class 23, high rise class 32, and high cut-off class 41 may be made to result in an overall correction of the algebraic total of the classes as follows:

	40	55	70	130	300	500	1000	2000	3000	5000	7000	8000
Class 11	1.6	0.8	0.6	0	0	0	0					
" 23	-4.2	-4.0	-3.8	-2.0	-0.4	0	0					
" 32								-0.8	-1.6	-3.2	-4.4	-4.8
" 41								0	1.0	3.6	5.6	
Total	-2.6	-3.2	-3.2	-2.0	-0.4	0	0	-0.8	-1.6	-2.2	-0.8	+0.8

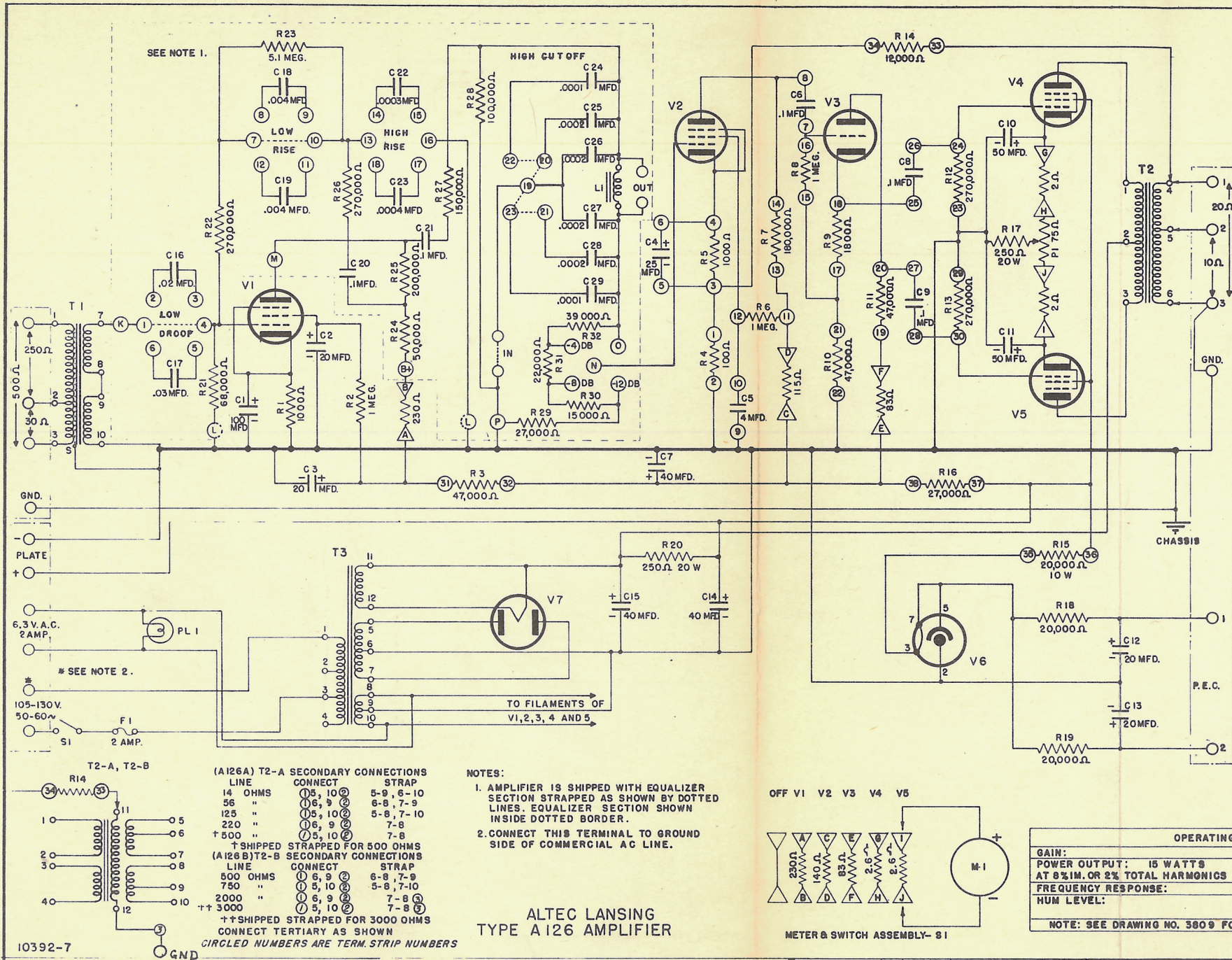
As shipped the strappings are: 10-20-30-44

When equalization is required of less than all 4 sections, the remaining and unused sections must be strapped for flat response.

CORRECTION FACTORS FOR EQUALIZER STRAPPING FREQUENCY

Section	Class	Strapping	40	55	70	130	300	500	1000	2000	3000	5000	7000	8000
Low Droop	10	1-4	0	0	0	0	0	0	0	0	0	0	0	0
	11	1-2,6,3-4-5	+1.6	+0.8	+0.6	0	0	0	0	0	0	0	0	0
	12	1-6,4-5	+3.2	+2.0	+1.2	0	0	0	0	0	0	0	0	0
	13	1-2,3-4	+5.6	+4.0	+2.8	+1.0	0	0	0	0	0	0	0	0
	14	1-2,3-6,4-5	+9.8	+7.2	+4.2	+2.4	+0.2	0	0	0	0	0	0	0
Low Rise	20	7-10	0	0	0	0	0	0	0	0	0	0	0	0
	21	7-8-12,9-10-11	-2.0	-1.2	-0.4	0	0	0	0	0	0	0	0	0
	22	7-8,9-10	-4.0	-2.8	-2.2	-0.8	0	0	0	0	0	0	0	0
	23	1-2,6,3-4-5,7-8,13-9,11-10	-4.2	-4.0	-3.8	-2.0	-0.4	0	0	0	0	0	0	0
	24	7-8,9-12,10-11	-5.6	-5.2	-4.4	-2.4	-0.6	0	0	0	0	0	0	0
High Rise	30	No straps on 13 and 16							0	0	0	0	0	0
	31	13-14,15-18,16-17						0	-0.2	-0.8	-2.0	-2.8	-3.2	
	32	13-14,15-16						0	-0.8	-1.6	-3.2	-4.4	-4.8	
	33	13-18,16-17						0	-1.2	-2.4	-4.0	-5.6	-6.2	
	34	13-14-18,15-16-17						0	-2.4	-3.8	-5.4	-5.6	-5.8	
High Cut Off	40	Out						0	0	0	0	0	0	
	41	1-4,7-10 In						0	0	+1.0	+3.6	+5.6		
	42	19-22-23 In						0	0	0	+1.4	+5.2	+8.0	
	43	19-20-21 In						0	0	+0.4	+1.6	+7.6	+11.2	
	44	19-20-21-22-23 In						0	0	+0.2	+2.4	+9.6	+13.2	

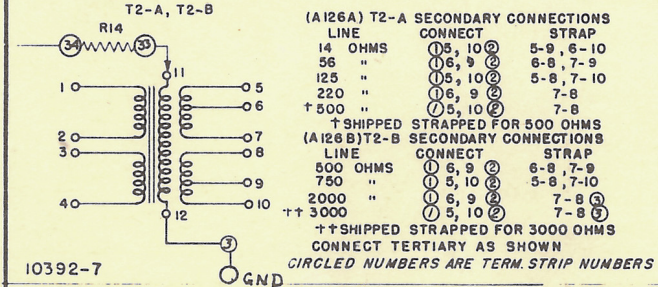




**PARTS LIST**

C1	100 MFD. 25 V.D.C.
C2, 22, 23	20X20 MFD. 450 V.D.C.
C4	25 MFD. 25 V.D.C.
C6	4 MFD. 350 V.D.C.
C6, 8, 9	.1 MFD. 600 V.D.C.
C10, 11	80X50 MFD. 150V.D.C.
C14, 15	40X40 MFD. 450V.D.C.
C16	.02 MFD. 600 V.D.C.
C17	.03 MFD. 600 V.D.C.
C18, 19	.004 MFD. 300 V.D.C.
C20, 21	.1 MFD. 600 V.D.C.
C22	.0003 MFD. 500 V.D.C.
C23	.0004 MFD. 500 V.D.C.
C24, 25	.0001 MFD. 500 V.D.C.
C26, 27, 28	.0002 MFD. 500 V.D.C.
R1, 5	1000 OHMS 1/2 WATT
R2, 6, 8	1 MEG OHM "
R3, 24	47,000 OHMS "
R4	100 "
R7	180,000 " 1
R9	1800 " 1/2 "
R10, 11	47,000 " 1 "
R12, 13	270,000 " 1/2 "
R14	12,000 " "
R15	20,000 " 10 "
R16	27,000 " 1 "
R17, 20	250 " 20 "
R18, 19	20,000 " 1/2 "
R21	68,000 " "
R22, 26	270,000 " "
R23	5.1 MEG OHMS "
R25	200,000 OHMS 3/4 "
R27	150,000 " 1/2 "
R28	100,000 " "
R29	27,000 " "
R30	15,000 " "
R31	22,000 " "
R32	39,000 " "
A-B	ALTEC LANSING 250 OHMS
C-D	PRECISION 140 "
E-F	RESISTORS 85 "
G-H	RESISTORS 2.6 "
I-J	PER DWG. 3884 2.6 "
L1	ALTEC LANSING TYPE TA 325
T1	" " T88103
T2	" " TL 217
T2-A	" " TL 216
T3	" " TJ 604
V1, V2	1620 (6J7 MAY BE SUB'D FOR V2)
V3	6J6
V4, V5	6L6G
V6	OC3
V7	5U4G
F1	2 AMP. TYPE 3A6
S1	CENTRALAB 1411 6 POS. 2 CIR.
M1	ALTEC LANSING 1/2 METER PER DRAWING 3679
P1	75 OHMS IRC W-75
PL1	GE MAZDA NO. 44
S2	H & H NO. 81715 S.P.S. T.
T2-B	ALTEC LANSING TYPE TL 219
R24*	50,000 OHMS 3/4 WATT

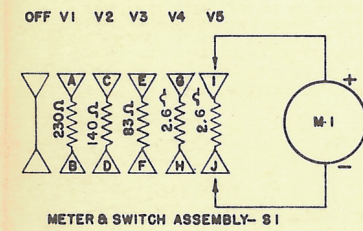
\*USE S.S.WHITE NOISE TESTED RES.



**NOTES:**

- AMPLIFIER IS SHIPPED WITH EQUALIZER SECTION STRAPPED AS SHOWN BY DOTTED LINES. EQUALIZER SECTION SHOWN INSIDE DOTTED BORDER.
- CONNECT THIS TERMINAL TO GROUND SIDE OF COMMERCIAL AC LINE.

**ALTEC LANSING  
TYPE A126 AMPLIFIER**



**OPERATING DATA**

GAIN:	90 DB AT 1000 C.P.S.
POWER OUTPUT:	+34 DB (.006 W. REF. LEVEL) AT 8% TH. OR 2% TOTAL HARMONICS
FREQUENCY RESPONSE:	+1.8 DBM (.001W. REF. LEVEL) ± 1 DB. 20 TO 20,000 C.P.S.
HUM LEVEL:	-35 DB. (.006 W. REF. LEVEL) -27.2 DBM. (.001 W. REF. LEVEL)

NOTE: SEE DRAWING NO. 3809 FOR POWER CURVE.

10392-7

REDUCE TO 9" LONG AND TRIM TO THIS LINE

PRINTED IN U. S. A.

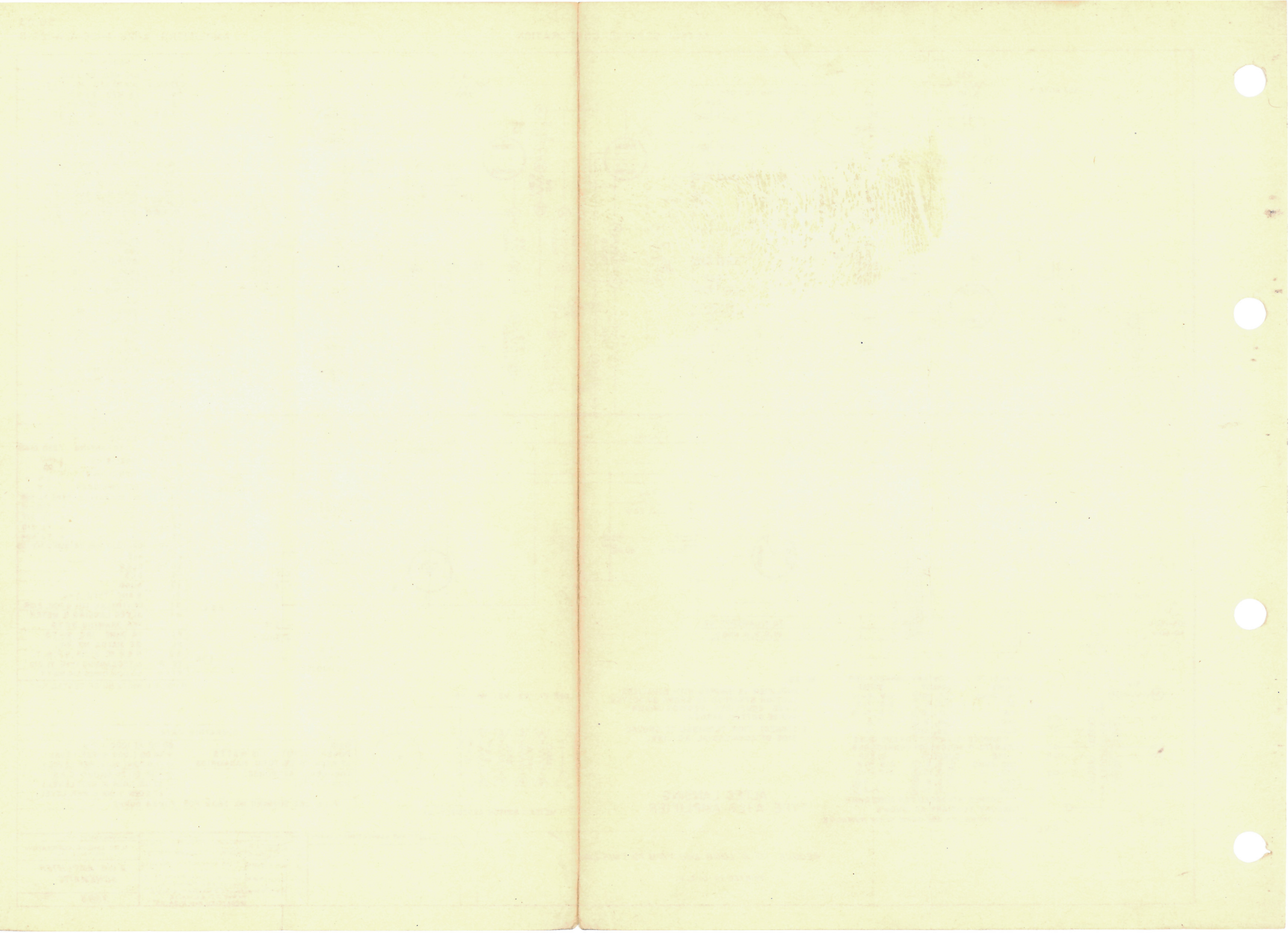
ISSUE	APPROV	DATE	REVISION	CHANGES	DR. BY	APP'D
7	CHM	7-5-54		EXPANDED REPAIRS SECTION		
8	CHM	8-5-54		REVISED TERM. CHANGES TO S1		
9	CHM	8-10-54		T2-A CONNECTIONS CHANGED		
10	CHM	9-2-54		CONNECTIONS SHOWN TO EQUALIZER TERMINAL		
11	CHM	9-30-54		SHIPPED WITH 1500 OHMS WIRE 2% S.S. WHITE SPECIFIED FOR R-24, 25		

ALTEC LANSING CORPORATION  
HOLLYWOOD, CALIF.

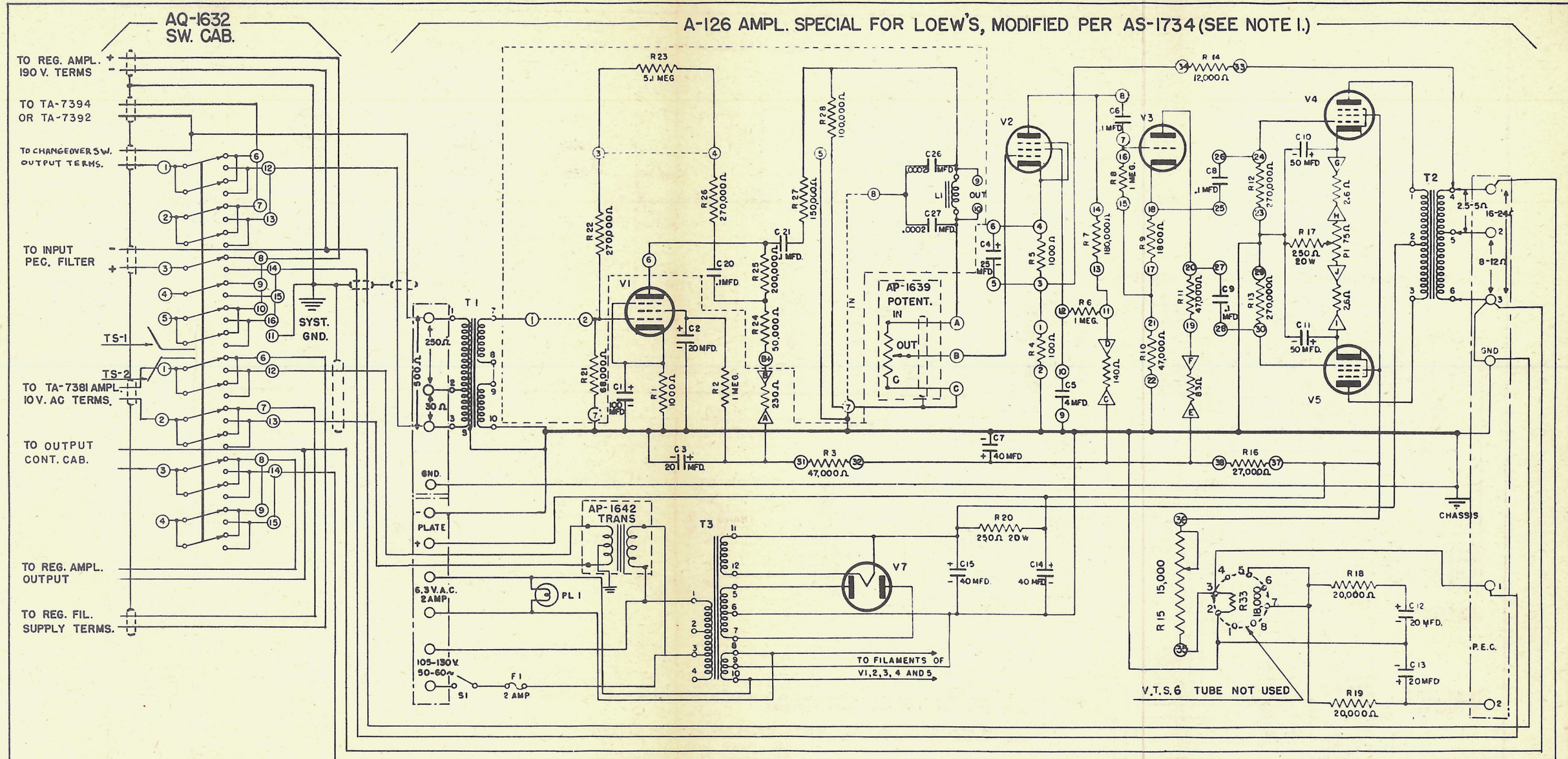
**A 126 AMPLIFIER  
SCHEMATIC**

3885









NOTE 1: THE A-126 AMPLIFIER, SPECIAL FOR LOEW'S MODIFIED PER AS-1734 SAME AS STANDARD A-126 EXCEPT FOR THE FOLLOWING:

ADDED

R-15 15,000 OHM, 25 WATT, ADJUSTABLE  
R-33 18,000 " 10 "  
AP-1639 POTENTIOMETER  
AP-1642 TRANSFORMER

REMOVED

R-15 20,000 OHM, 10 WATT  
R-29 27,000 " 1/2 "  
R-30 15,000 " 1/2 "  
R-31 22,000 " 1/2 "  
R-32 39,000 " 1/2 "  
V-6 6G-3 TUBE

ISSUE 1 6-30-57 APP'D *WJH*

DRAWN BY *WJH* DATE 6-30-57  
DATE *9/5*

AQ-1624 EMERGENCY MAIN AMPL. SYSTEM  
W.E. INSTALLATIONS (USING TA-7381 AMPLS.)  
SCHEMATIC  
FOR LOEW'S THEATRES

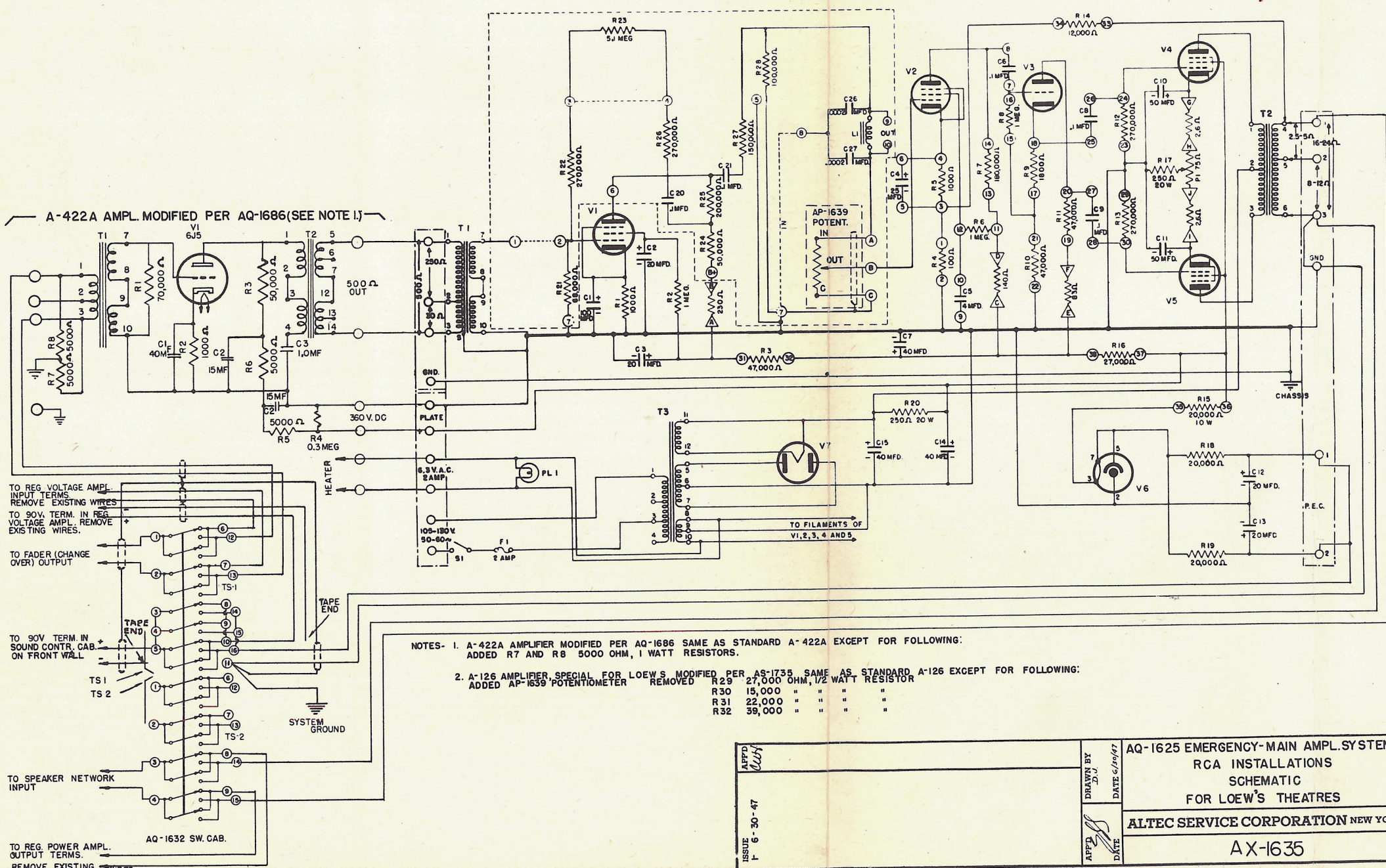
ALTEC SERVICE CORPORATION NEW YORK

AX-1634



A-126 AMPL. SPECIAL FOR LOEW'S, MODIFIED PER AS-1735(SEE NOTE 2)

A-422A AMPL. MODIFIED PER AQ-1686(SEE NOTE 1)



TO REG. VOLTAGE AMPL. INPUT TERMS REMOVE EXISTING WIRES  
 TO 90V. TERM. IN REG. VOLTAGE AMPL. REMOVE EXISTING WIRES.  
 TO FADER (CHANGE OVER) OUTPUT  
 TO 90V TERM. IN SOUND CONTR. CAB. ON FRONT WALL.  
 TS1  
 TS2  
 TO SPEAKER NETWORK INPUT  
 TO REG. POWER AMPL. OUTPUT TERMS. REMOVE EXISTING WIRES

- NOTES- 1. A-422A AMPLIFIER MODIFIED PER AQ-1686 SAME AS STANDARD A-422A EXCEPT FOR FOLLOWING:  
 ADDED R7 AND R8 5000 OHM, 1 WATT RESISTORS.
2. A-126 AMPLIFIER SPECIAL FOR LOEW'S MODIFIED PER AS-1735 SAME AS STANDARD A-126 EXCEPT FOR FOLLOWING:  
 ADDED AP-1639 POTENTIOMETER  
 REMOVED
- |     |                               |
|-----|-------------------------------|
| R29 | 27,000 OHM, 1/2 WATT RESISTOR |
| R30 | 15,000 " " " "                |
| R31 | 22,000 " " " "                |
| R32 | 39,000 " " " "                |

APPD DATE 6-30-47	DRAWN BY D.J. DATE 6/17/47	AQ-1625 EMERGENCY-MAIN AMPL. SYSTEM RCA INSTALLATIONS SCHEMATIC FOR LOEW'S THEATRES
		ALTEC SERVICE CORPORATION NEW YORK AX-1635



1. PURPOSE - Hum reduction in Altec Lansing Amplifier Systems.
2. A-421 Cathode Follower, 721 Control Cabinet & A-126 Amplifier.  
Both the ground and hot side of the A-421 should be carried to the respective change-over cabinets in two conductor shielded wires which has an outer cloth or rubber covering so that its shield is insulated from the other shields. The common terminal of each 721 Cabinet should go to the ground position on the A-126 Amplifier in such a way that the only circuit ground for all three of these items is at the A-126 Amplifier.
3. A-420, A-422 and A-422-A Amplifiers. - The strap between "-Plate" terminal and the chassis ground lug should be removed. All pre-amplifiers now shipped from the factory have this modification. The "-Plate" of the pre-amplifiers will go to ground through the power supply.
  - 3.1 Additional hum reduction may be obtained in the A-422 and A-422-A Amplifiers by replacing Resistor R-8, 10,000 ohms with 2 - 5000 ohm resistors connected in series. Disconnect 1 - 15 mf section of C-2 and connect to the junction of the 2 - 5000 ohm resistors.
4. A-126 Amplifier - The ground lug on the lower left hand terminal strip is the main ground. This lug may also be used as "-Plate" as it is strapped internally to the "-Plate" terminal on the lower right hand terminal strip. On early amplifiers the ground lug on the upper left hand terminal strip should be used only to ground the shield of input cable or one side of input line, if that is required. New A-126 Amplifiers have the ground lugs on the upper left hand and lower left hand terminal strips tied together so that they may be used indiscriminately.





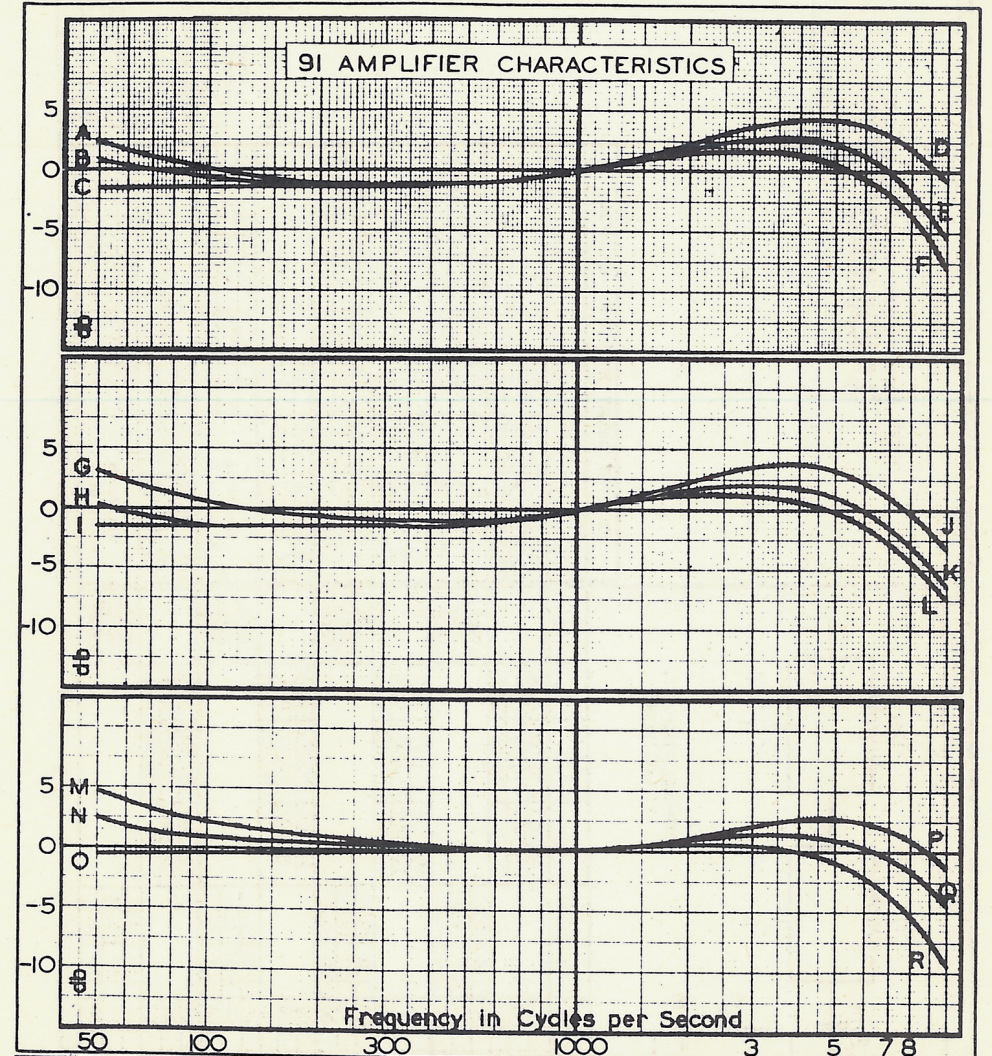










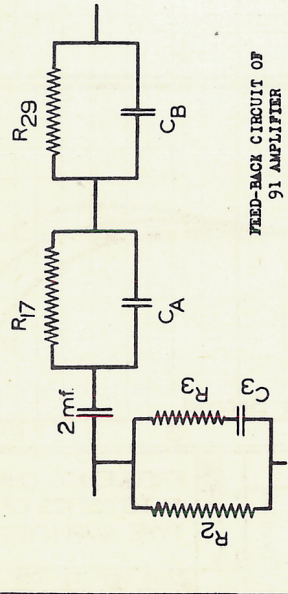


ISSUE 1: 1-28-38 M.P.F. L.S.P.	AQ-8337-1 ASSOC. DRAWING	CH. 1 ENGR. [Signature] DR. [Signature]	FREQUENCY CHARACTERISTICS OF 9I TYPE AMPLIFIER. ALTEC SERVICE CORP. N. Y. AQ-8337-A PRINTED IN U.S.A.
--------------------------------------	-----------------------------	---	--



ISSUE: 1-28-58 MFP

NOTE: Response runs should be made with 91 amplifier terminated in 12 ohm non-inductive resistor.

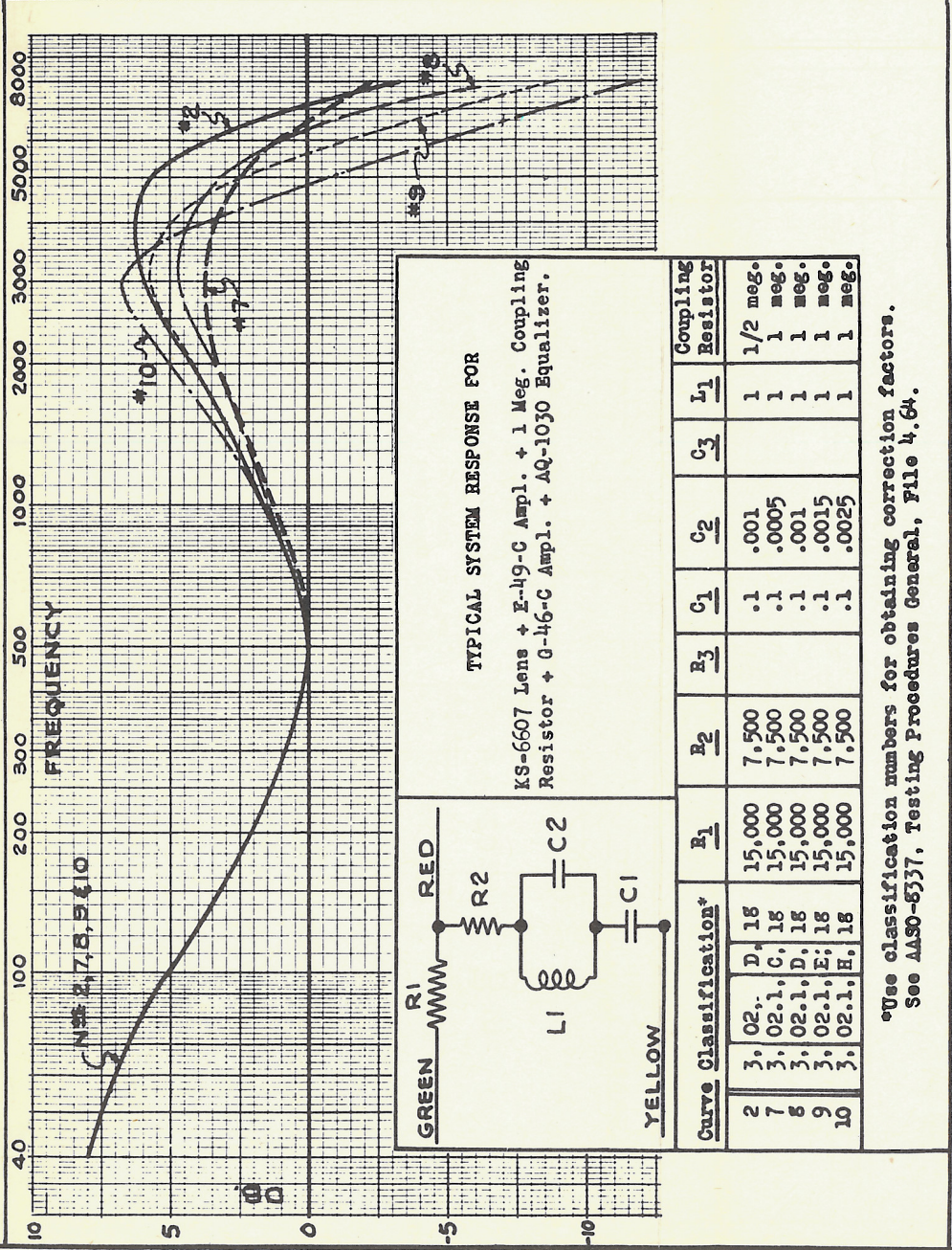
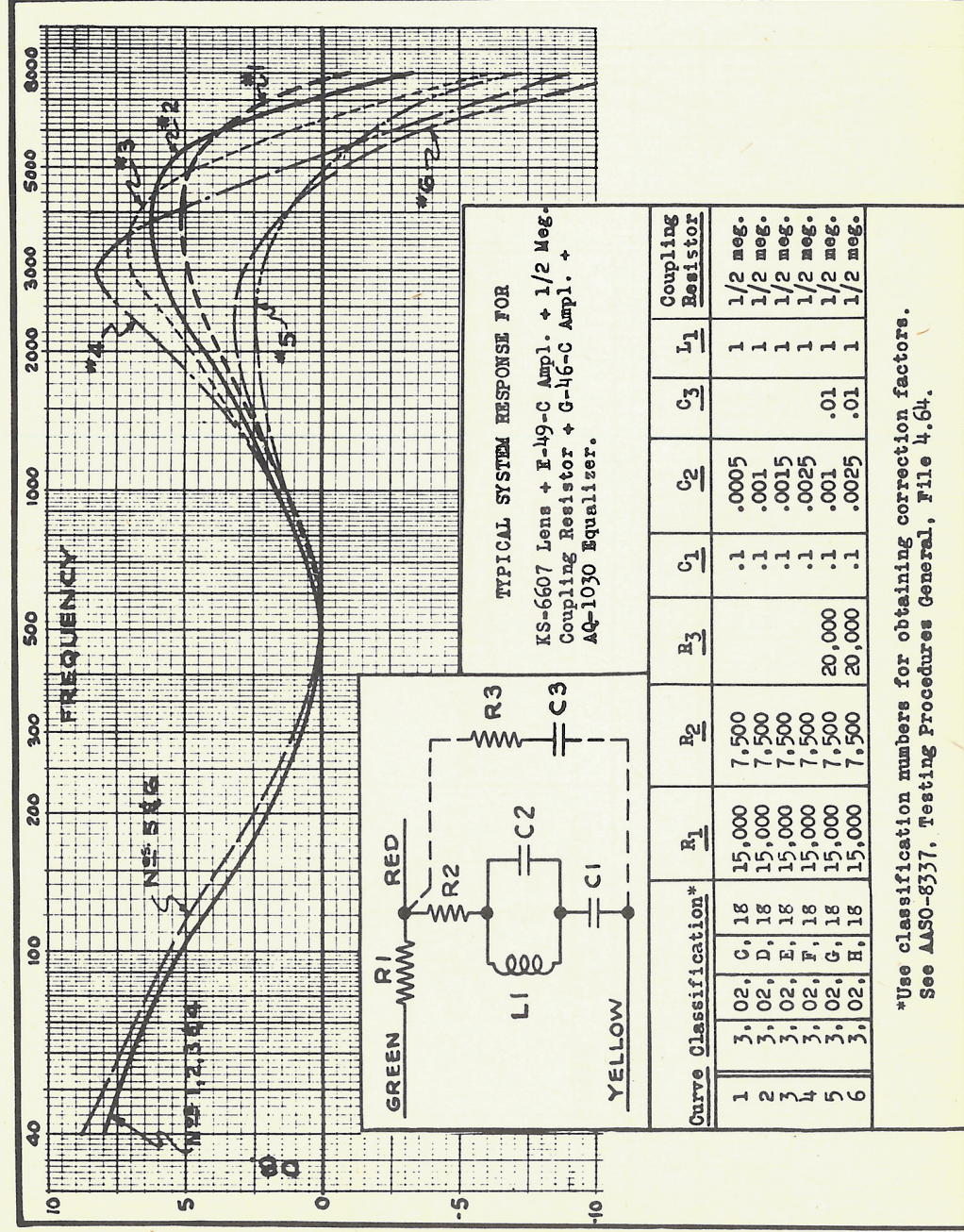


1000 ~ GAIN	RESPONSE CORRECTIONS FOR 91 AMPLIFIER																
	CURVE	R <sub>2</sub>	R <sub>3</sub>	C <sub>3</sub>	R <sub>17</sub>	R <sub>29</sub>	C <sub>A</sub>	C <sub>B</sub>	55	130	300	1000	3000	5000	7000	8000	
93.0	A	350			70,000	70,000	0.05		-2.1	0	+0.9	0					
	B	350			70,000	70,000	0.1		-0.8	+0.8	+1.0	0					
	C	350			0	70,000	open		+1.4	+1.4	+1.1	0					
	D	350	150	0.2				open	Use Curve D, E, or F								
	E	350	150	0.2				.0003	Use Curve								
	F	350	350	0.2				.0003	A, B, or C								
	G	400			150,000	150,000	0.05		-2.5	0	+0.8	0					
98.6	H	400			150,000	150,000	open		0	+1.5	+1.5	0					
	I	400			0	150,000	open		+1.4	+1.5	+1.5	0					
	J	400	150	0.2				.0001	Use Curve J, K, or L								
	K	400	300	0.2				.0001	Use Curve								
	L	400	500	0.2				.0001	G, H, or I								
	M	200			40,000	40,000	0.05		-4.0	-1.6	-1.0	0					
	N	200			40,000	40,000	0.1		-2.0	+6.0	+0.5	0					
93.8	O	200			0	40,000	open		+0.5	+0.3	0						
	P	200	200	0.2			open	Use Curve									
	Q	200	500	0.1			open	M, N, or O									
	R	200	500	0.1			.0005	Use Curve									
	M	200			100,000	100,000	0.02		-4.0	-1.6	-1.0	0					
	N	200			100,000	100,000	0.04		-2.1	+0.6	+0.5	0					
	O	200			0	100,000	open		+0.5	+0.3	0	0					
101.1	P	200	100	0.2			open	Use Curve P, Q, or R									
	Q	200	300	0.15			open	Use Curve									
	R	200	300	0.2			.00025	M, N, or O									
	M	200			100,000	100,000	0.02		-2.0	-2.6	-1.8	0					
	N	200			100,000	100,000	0.04		-1.5	-1.0	+0.5	0					
	O	200			0	100,000	open		-0.5	+1.0	+3.6	0					
	P	200	100	0.2			open	Use Curve P, Q, or R									

AQ-8337-1 Correction Factors ASSOCIATED DRAWINGS

FREQUENCY CHARACTERISTICS OF 91 TYPE AMPLIFIER.  
ALTEC SERVICE CORP N.Y.  
AQ-8337-B  
PRINTED IN U.S.A.





DATE: 1-18-39  
DRAWN BY: E. J. Kennedy  
DATE: 1-10-39

TYPICAL SYSTEM  
RESPONSE  
AQ-1030 EQUALIZER  
WITH 46 TYPE AMPL.

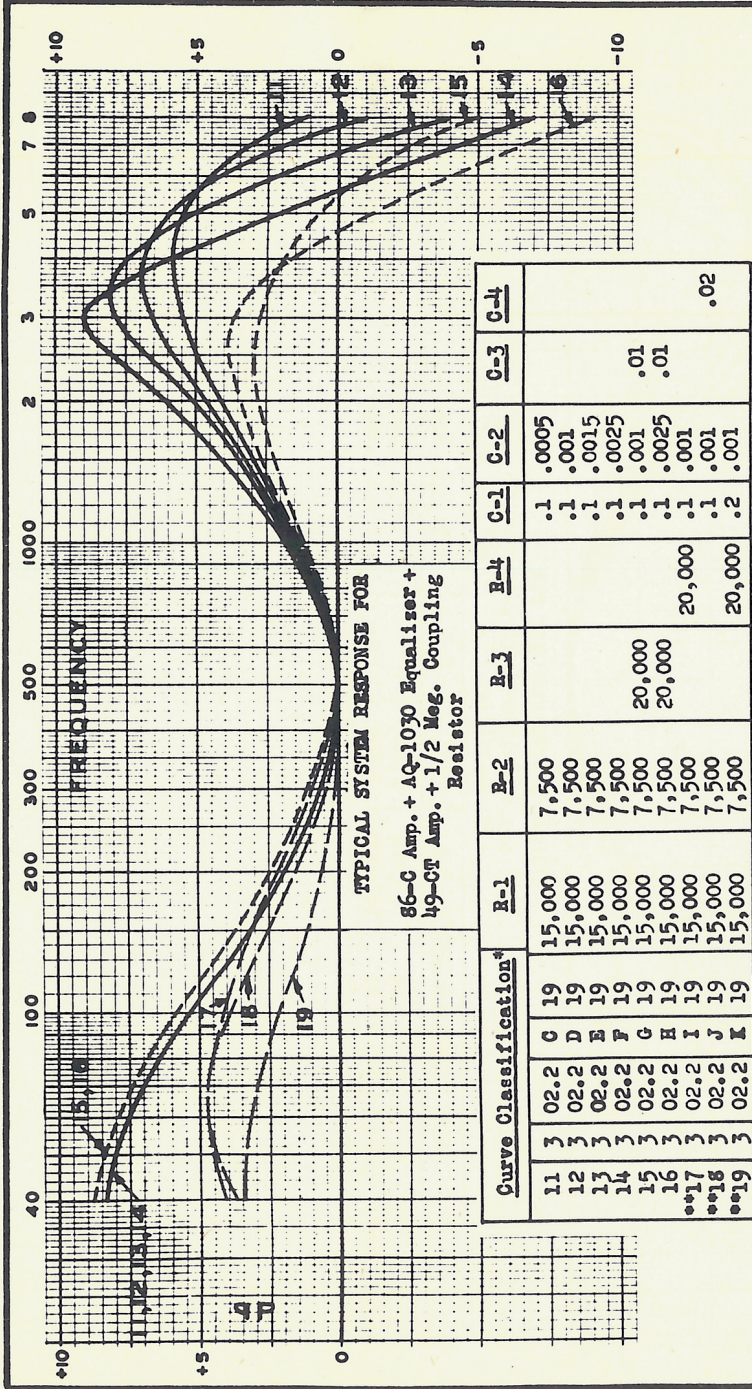
ALTEC SERVICE CORPORATION  
NEW YORK

AQ-8337-C

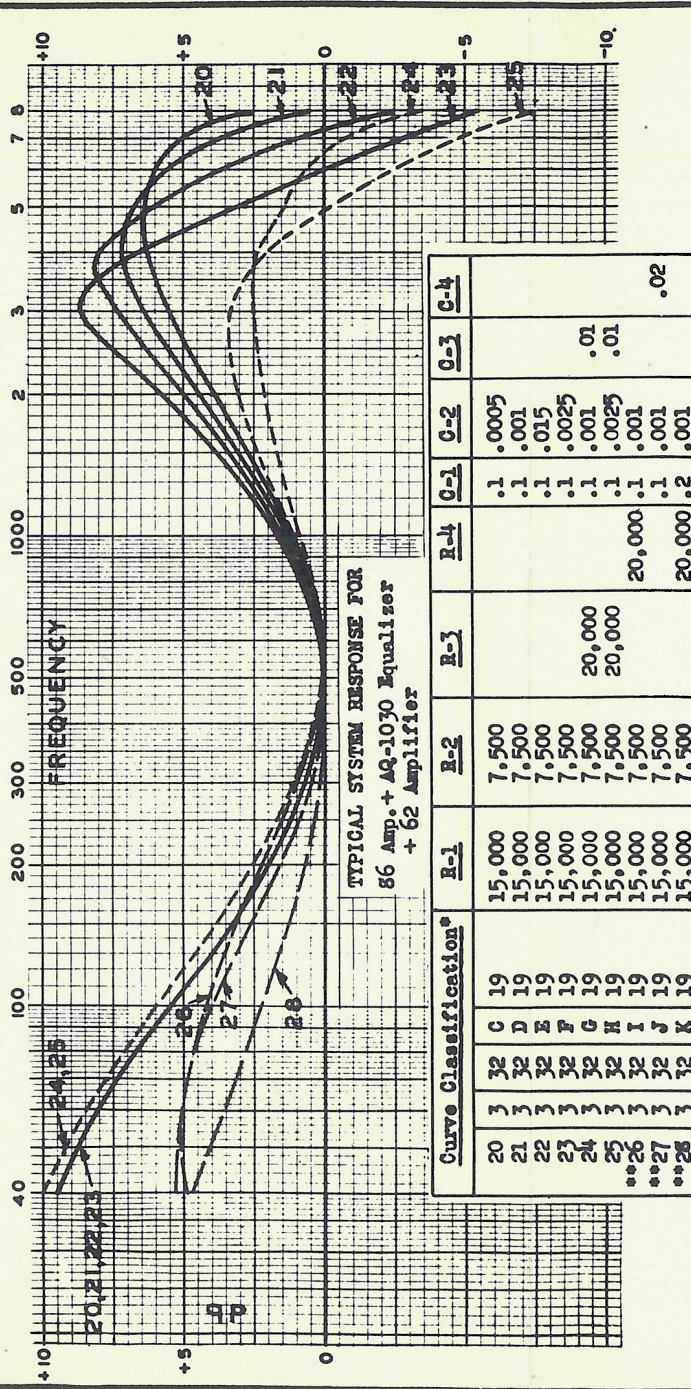
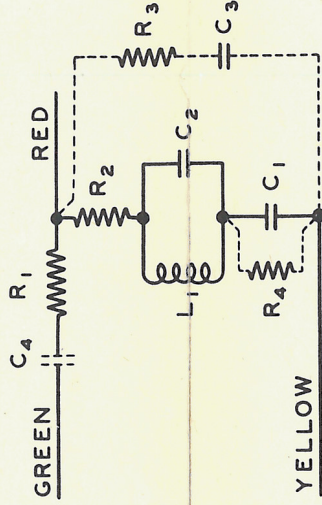








\*Use classification numbers for obtaining correction factors - See AASO-8337-2  
Testing Procedures General, File 40.64.



\*\*I, J, and K are low-end curves only and independent of C-2. The value of C-2 will determine which high-end curve, G, D, H, or F, is combined with the selected low-end curve.

11-10-38 APP'D  
WMS

APP'D R.C.S.  
DRAWN BY  
KEYNICK  
DATE 11-10-38

TYPICAL SYSTEM  
RESPONSE  
AQ-1030 EQUALIZER  
WITH 86 TYPE AMPL.  
ALTEC SERVICE CORPORATION  
NEW YORK  
AQ-8337-D







## 1. INTRODUCTION

- 1.1 The variety of equalizer curves which satisfies all possible requirements is, of course, limitless. To realize most of such curves would require complicated network configurations and the design mathematics would be extremely involved. Furthermore, since coils would very often be required, it would frequently be very difficult or time-consuming to obtain the required elements.
- 1.2 There is a type of equalizer, however, employing only resistors and condensers, the design of which can be readily calculated from charts. Such equalizers are of particular value in the field since the elements are readily available, the design can be completed in a few minutes, and their properties are such that a large part of the equalizer problem can be solved with them. The purpose of this memorandum is to describe the methods of design of such equalizers.

## 2. DESCRIPTION OF CURVES

- 2.1 The curves obtainable from these two-terminal R-C equalizers are given on AP-1076, attached. There are four general types:
- 2.11 Low Droop or High Rise. (The difference is only a matter of location on the frequency axis.) Note that this family of curves is flat at the low and high extremities and rises with frequency over an intermediate range. These curves are distinguished from each other by overall db difference between the transmission at the two extremities and by the "Frequency of the half-way point". The curves are drawn with the half-way point falling at 1000 cps., but this point may be shifted to any frequency by proper choice of the elements used. A particular curve labeled "LD 6 db,  $f_{1/2} = 400$  cps." has 6 db overall difference between extreme highs and extreme lows, and at 400 cps. the transmission is 3 db above the extreme lows or 3 db below the extreme highs. LD or HR curves are obtained by a parallel R-C pair connected in series with the line.
- 2.12 Low Rise or High Droop. These curves have the same shape as the LD, HR curves but drop off as frequency rises. They are obtained by connecting a series R-C pair across the line.
- 2.13 High Cutoff. Sharp cutoffs are not given by these curves but either the "single" or the "double" serves in most cases. The "single" curves are defined by the frequency at which transmission is down 3 db, and the "double" curves by the frequency of 6 db attenuation. The "single" cutoff is obtained by connecting a condenser across the line. The "double" cutoff is provided by two similar "single" cutoffs at isolated parts of the circuit.
- 2.14 Low Cutoff. These are similar to the high cutoffs but affect the low end of spectrum. The "single" low cutoff is obtained by connecting a condenser in series with the line.

## 3. METHOD OF DESIGN

- 3.1 An equalizer design problem usually begins with two curves: the response of the system unequalized, and the desired response. Subtract the actual from the desired characteristic to obtain the required insertion characteristic of the equalizer. Plot this to the same scale as AP-1076.
- 3.2 By inspection, determine which curve type on AP-1076 best fits the required insertion characteristic. Place the sheet containing the required insertion curve over AP-1076; hold the combination between the eye and a light source; adjust the two sheets, keeping the 0 db axis of both sheets aligned, until the best fit of some curve of AP-1076 with the insertion curve is obtained. Note the number of db overall of the selected curve on AP-1076 and the frequency at which its half-way point (1000 cps. on AP-1076) falls on the scale of the insertion curve. Call this the "frequency of the half-way point."
- 3.3 We have now found the values of "DB Overall" and "frequency of the half-way point" of the desired curve. One additional item must be evaluated: the value of  $R_0'$  for LR, HD or HC or the value of  $R_0 + R_L$  for LD, HR or LC. These values apply to the circuit into which the equalizer will be connected.
- (a)  $R_0'$  is the parallel combination of all impedances to ground at the part of the circuit across which (to ground) the equalizer will be connected. This section begins with the plate of a tube or a loss device like a fader and the grid of the next tube or a loss device.
- (b)  $R_0 + R_L$  is required when the equalizer is inserted in series with the ungrounded side of the circuit.  $R_0$  is the parallel combination of the impedances to the left (toward the source) and  $R_L$  is the combination of impedances to the right of the point where the equalizer will be inserted.



TESTING PROCEDURES, GENERAL  
 TWO-TERMINAL, R-C EQUALIZER DESIGN

Example: An HD equalizer is to be inserted between V1 and V2 of the 46 type amplifier. Combine the plate impedance (15,000 ohms) of V1, the plate feed resistance (100,000 ohms) and the resistance of the voltage divider (180,000 ohms) all in parallel. This gives a value of 12,000 ohms for  $R_0'$ . If HR or LD or LC is required, combine 12,000 and 100,000 ohms in parallel to obtain 13,000 ohms for  $R_0$ , and, since  $R_L$  is 180,000 ohms,  $R_0 + R_L$  is 193,000 ohms.

- (c) When it is more convenient to measure than compute these values, the procedure is as follows: Connect a variable resistance between the two points to which the proposed equalizer will be connected. Vary the resistance until the signal at the system output drops 6 db. The resistance at this setting equals the value of  $R_0'$  or of  $R_0 + R_L$ . A 120 cycle signal is usually suitable for this purpose. This method should always be used when the equipment is available for the measurement. When the equalizer is to be connected in series in the line, the line must, of course, be opened to obtain the two points for the measurement.
- 3.4 If a LR, HD or a LD, HR curve meets the requirements, AP-1074 and 1075 may now be used to evaluate the resistor and condenser required. Select the appropriate sheet and locate the slant line which is labelled with the full amplitude of the desired curve. Read the factor "A" on the left hand scale opposite the point where the selected slant line crosses the "frequency of the half-way point". Divide this factor by  $R_0'$  or  $R_0 + R_L$  (whichever applies) in Kilohms to obtain the capacity of the condenser in mf. Read the value of K from the selected slant line and multiply it by  $R_0'$  or  $R_0 + R_L$  in ohms to obtain the resistor value in ohms. The formulae given on AP-1074 and 1075 will minimize the danger of error in arithmetic.
- 3.5 If the requirements are best met with a cutoff curve, compute the required condenser value from the formulae:  
 Single HC -  $X_C = R_0'$ , or  
 $C = \frac{160,000}{f R_0'}$  mf., where f is the frequency of the 3 db point.  
 Single LC -  $X_C = R_0 + R_L$ , or  
 $C = \frac{160,000}{f(R_0 + R_L)}$  mf.
4. MISCELLANEOUS NOTES
- 4.1 Do not use the above methods within the feedback loop in feedback amplifiers.
- 4.2 Gain reserve must be available to accommodate any equalizer type which raises the response at the low or high end relative to the "voice-volume" range which is about 300 to 800 cps., and the amount of such reserve is equal to the elevation of either extremity relative to this mid-range. The droops and cutoffs introduce no volume loss unless the curve runs through the mid-region.
- 4.3 Distortion may result with LR or HD if a tube works into a low impedance, and in selecting a point for inserting an R-C pair for LR or HD do not cause a tube to work into an impedance less than its own plate impedance. Any handicap resulting from this prohibition can be removed with little or no gain loss by introducing a resistor in series with the line between the tube and the point of application of the equalizer. For example, assume the requirements call for a 10,000 ohm resistor and a .04 mf condenser based on insertion between grid and ground of V2 of the 86 type amplifier. Since V1 will be working into an impedance less than its own value above about 300 cps., this is an undesirable arrangement. However, if a 15,000 ohm resistor is connected in series with the grid, and the equalizer connected between the grid end of the resistor and ground, the tube will work into an impedance well above its own value. Naturally, the equalizer elements must be recalculated for the new value of  $R_0'$ .
- 4.4 Overloading will result from LR or HR if, due to loss in the equalizer, the level at the preceding tube is raised above the tube overload point. To determine whether this applies in a particular case, install only the equalizer resistor and increase the system input signal until full output is obtained. Overloading, if any, will be evidenced in the usual way.
- 4.5 The predicted curve will not be obtained if the circuit at the insertion point contains reactance. The design charts AP-1074 and 1075 are based on circuit impedances which are pure resistances. Reactance is encountered in three general forms:
- (a) Blocking (coupling) condenser between stages. These affect only the extreme low end and may usually be ignored.



- (b) A filter or equalizer already installed in the same portion of the circuit. In this case, either find another location for the proposed equalizer or determine experimentally the effect of a trial combination.
  - (c) A transformer. If unterminated on the far side, its impedance may be treated as infinite, except perhaps at extreme frequencies. The characteristic of the transformer will change if the impedance from which it works is changed. If this impedance is lowered, the transformer characteristic will rise at 5000-8000 cps. and if the impedance is increased it will fall in the same region. The amount depends upon the transformer. If the transformer is loaded substantially, the reflected impedance may be assumed to apply.
- 4.6 The curves AP-1076 were drawn with the frequency of the half-way point at 1000 cps. to facilitate their interpretation for any frequency by multiplying the frequency scale by a factor: e.g., to shift from 1000 to 300 cps. multiply all abscissae by 0.3. A more convenient method is to use a folded blank sheet having the same log scale as AP-1076, placing this under the curves so that 300 cps. on the blank sheet corresponds to 1000 cps. on the plotted sheet. All points on the curves may then be read off above this adjustable frequency scale.



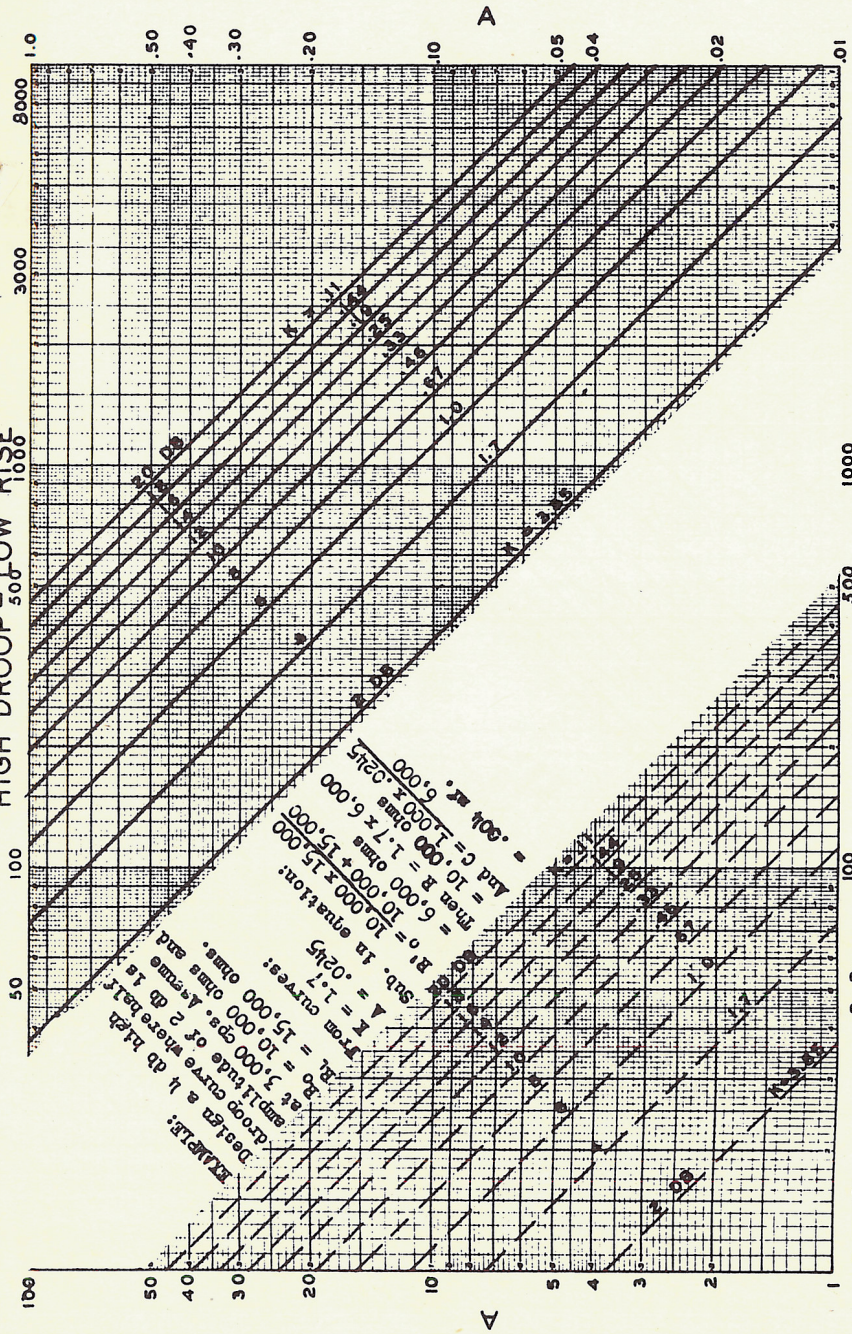






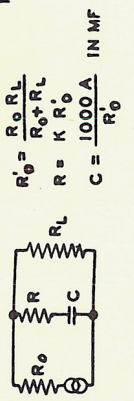


TWO TERMINAL EQUALIZER DESIGN  
HIGH DROOP 50% LOW RISE 10%

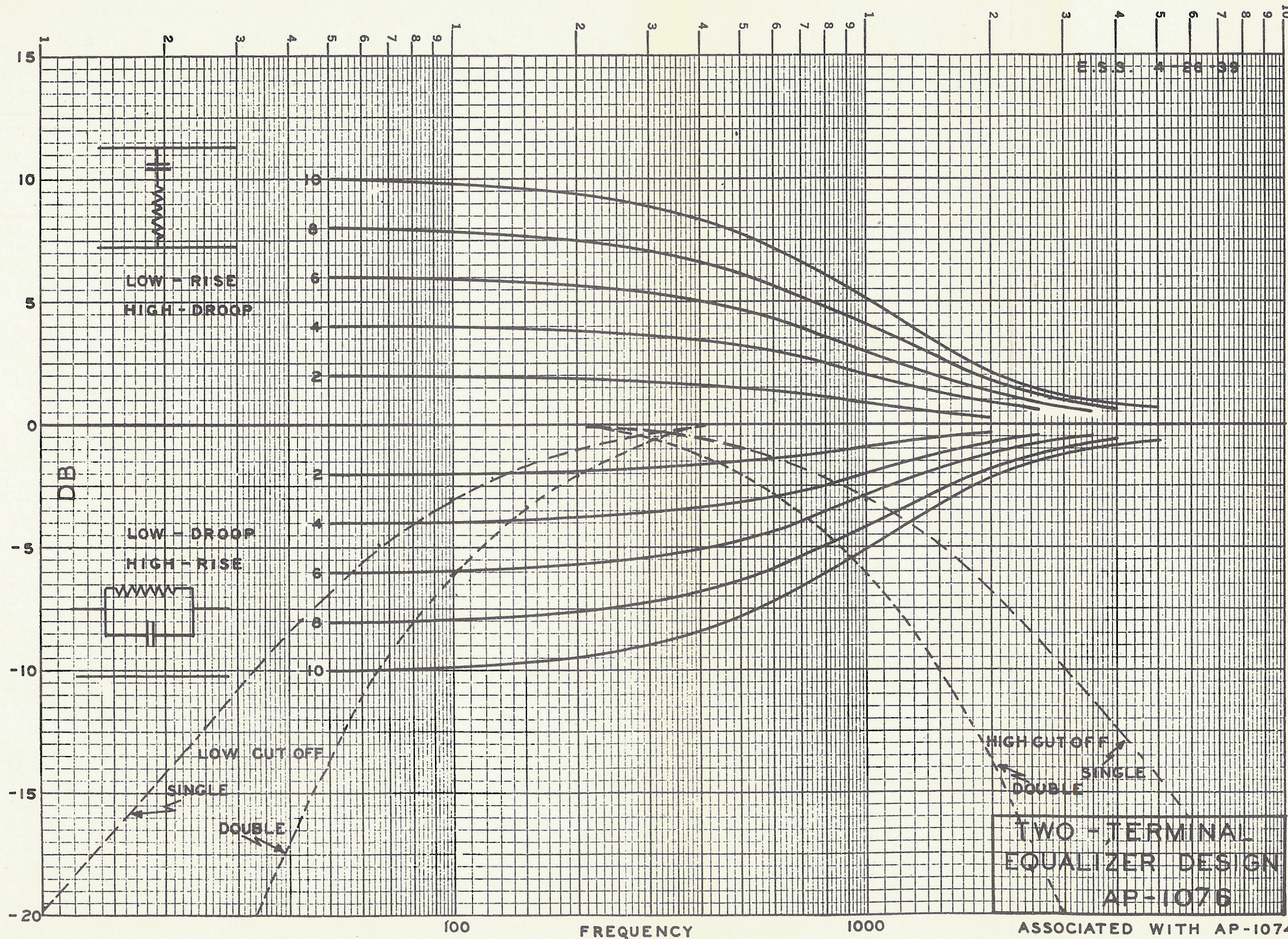


AP-1075  
ASSOCIATED WITH AP-1076  
4-26-39 E.S.S.

FREQUENCY OF HALF AMPLITUDE  
(FULL AMPLITUDE GIVEN ON CURVES)













1. ABSTRACT Replaces Addendum #5, "Testing Procedures, General" (4.604)

1.1. The Transmission Test, Intermediate Points, is for use where the usual methods are unsuccessful in bringing a system within limits of gain or response. It facilitates the identification of the particular part or parts which are functioning abnormally.

1.2 References: The drawings associated with Testing Procedures, General, File 4.604.

1.3 Test Equipment and Materials Required.

Form ERPI-596  
Multi-frequency test reel  
1000 cps - 8000 cps test loop

TA-7310 Test Amplifier  
TA-4145 Output Meter

## 2. PROCEDURE

2.1 This test is similar to that of the full-system transmission test except, in this test: (a) two frequencies only will be considered; (b) readings will be taken not merely at the system output, but at any selected point within the system; and (c) Variations from Normal will be derived which apply to that portion of the system between the test film and the Point of Measurement. By comparing the Variations from Normal at consecutive points, the local circuit in which the irregularity exists will be readily discovered.

2.2 The system is set up to provide readings of convenient value (see Sect. 3); the test amplifier is connected at the Point of Measurement (4.); the calibrated test loop is reproduced (5.), and the readings recorded on form ERPI-596. Corrections for the system components prior to the measurement point (6.) are entered on the form and the Variation from Normal derived in the usual way.

3. GAIN SETTINGS - The following settings, together with the test amplifier R-2 values listed on ASP-6244, will normally provide levels easily read on the TA-4145 Output Meter yet below the gain-load point (8 db) of the test amplifier.

3.1 Set the exciter lamp current at approximately -5 db level (3.2 amperes for the 4 amp. lamp) (see ASP-6237).

3.2 Set all attenuators on Step "1" (0 loss).

3.3 Set the fader for approximately 15 db loss (see ASP-6240).

3.4 Set the gain control of 46 type Amplifiers at -15 db.

Note: Normally, with these settings, the 1000 cps reading at the output of the film amplifier will be around 0 db, using the test amplifier 1/2 meg. R-2 resistor. If this level is not obtained the exciter lamp current may be readjusted to approach this value.

## 4. TEST AMPLIFIER CONNECTIONS

4.1 (Refer to Sect. 3 of E.B. "TA-7310 Test Amplifier", Issue #1, File 4.03). Connect the input terminal of the test amplifier to the "Point of Measurement" with as short a lead as possible. (Connect the test amplifier ground connection to the ground terminal of the amplifier under test.) Switch D1 should be in "Test" position and resistor R2 selected as indicated on ASP-6244.

4.2 When measuring at the input of the film amplifier (PEC terminal) a mica condenser (.005 mf to 0.1 mf) must be connected in series with the test amplifier input lead to avoid a dc flow through the test amplifier input circuit and the accompanying reduction of PEC polarizing voltage. This condenser will not appreciably change the test amplifier calibration corrections at 1000 cps or above. Do not disconnect the PEC lead at the anode terminal block nor throw D2 switch to "PEC".

4.3 When measuring at the output of the film amplifier, it will be necessary to check the terminals to find which one is ungrounded. If neither terminal is grounded a temporary ground connection should be made for this test. In the case of the 398 type Control Cabinet, due to the insertion of the balanced attenuation pad between the fader ground connection point and the film amplifier, it will be necessary to disconnect the cabinet, replace it with a 500 ohm resistance load, and make a temporary ground connection at one terminal of the amplifier. Normal connections should be restored for measurements at points beyond the fader.

## 5. TEST LOOP

5.1 The 1000-8000 cps dual frequency loop may be made from stock now carried by or available to all service inspectors. The recommended loop consists of about 4 feet of 1000 cps and 7 feet of 8000 cps film. The shorter 1000 cps strip serves to identify the frequency. In cases where the 1000 cps and 8000 cps sections reproduce at so near the same level as to render the change in frequency difficult to detect, about 6 inches on one end of the 8000 cps sound track may be blacked out with wax pencil or India ink in order that the V.I. needle will return to zero between sections.

5.2 To calibrate the loop, run it in the machine, follow with a regular test reel run and finally, rerun the loop to detect any changes in the system. Repeat this order if necessary, until consecutive loop runs check. (Space is provided on the form ERPI-596 for repeat runs if they are necessary.)

6. CORRECTIONS - The response corrections and gain values on ASP-6244 are valid for the R2 resistor values listed. Higher resistor values may be used without affecting the



## EQUIPMENT BULLETIN

validity of any of these figures except at those points where a bridging loss has been included as is indicated in the foot-notes on the drawing. If lower R2 values must be used, these may introduce a bridging loss which will require changes in the figures listed.

Bridging loss is the amount by which the level existing in the circuit prior to connecting a test amplifier is decreased when the test amplifier is bridged across the circuit. If a different resistor from the one specified is used, the bridging loss should be measured by taking readings at the system output before and after connecting in the test amplifier. The former reading (or response) minus the latter is the bridging loss in gain (or response). This value shall be used as follows to modify the "Gain, 1000 cps" or "Response Correction, 8000 cps" on ASP-6244.

"Gain, 1000 cps"

New gain value = tabulated gain + foot noted bridging loss in gain (if any) - measured bridging loss in gain.

"Response Correction, 8000 cps"

New response correction = tabulated correction - foot noted bridging loss in response (if any) + measured bridging loss in response.

## 7. MISCELLANEOUS NOTES

## 7.1 Points to be Measured.

(a) When the system output is not normal in response or gain, it may not always be necessary to check all intermediate points. Tests made at the film amplifier input (PEC terminal) furnish a check on the lens adjustment, the PEC sensitivity, and the grid resistors. A comparison of the "Variation from Normal" obtained from tests made at the film amplifier output and at the PEC terminal will give a check on the film amplifier as a whole from (but not including) the grid resistors to (and including) the fader input. Similarly, a comparison between the main amplifier output and the film amplifier output checks the main amplifier as a whole, plus the fader (except that faults in the input impedance of the fader will affect the film amplifier output reading, and hence, may not be revealed by this test).

(b) When thus the individual piece of equipment at fault is located, then checks should be made at the internal points of that unit. If there is an appreciable change in the "Variation from Normal" at two successive points, it is evident that there must be some abnormal condition affecting the second point. An analysis of the local circuit at that point will usually indicate the individual item at fault. A fault in any part of the local circuit to which the test amplifier is connected, may affect the readings. This local circuit must be considered as starting with the plate of one tube and ending at the grid of another tube. For instance, if the fault appears at the output of a 49 type Amplifier, but not at the V2 grid, the circuit involves the tube, the output transformer, the fader and the input transformer of the main amplifier. A check of the fader impedance (ASP-6248), and another measurement at the film amplifier output, terminated this time in a known 500 ohm resistor instead of with the fader, would serve to localize the fault. If the fault appears at the grid of the first tube in the main amplifier it may be the attenuators, the fader or the input transformer of the amplifier.

(c) Under normal conditions, the readings obtained at the grid of one tube of a push-pull stage should be duplicated at the other tube. However, a defect in only one half of the winding of the transformer feeding the push-pull stage may result in normal measurements at one tube grid, while measurements made at the amplifier output would be abnormal. Under such conditions a check at the grid of the other tube in the push-pull stage is desirable. There are sufficient blank spaces on the test form (ERPI-596) for such additional points, for points in additional main amplifiers, or for repeated readings. For instance, with the 41-42 amplifier combination, the column headed "V4 Grid" could be used for the grid of V1 tube in the 42 amplifier, while measurements at V2 of the 42 could be listed in one of the blank spaces. Likewise the measurements on a 43 amplifier may be listed in the blank spaces.

(d) Measurement is not recommended at the primary terminals of transformers. Readings at such points are subject to large variations, even with satisfactory transformers, and are no indication of the true effect of the transformer in the circuit.

## 7.2 Gain Test.

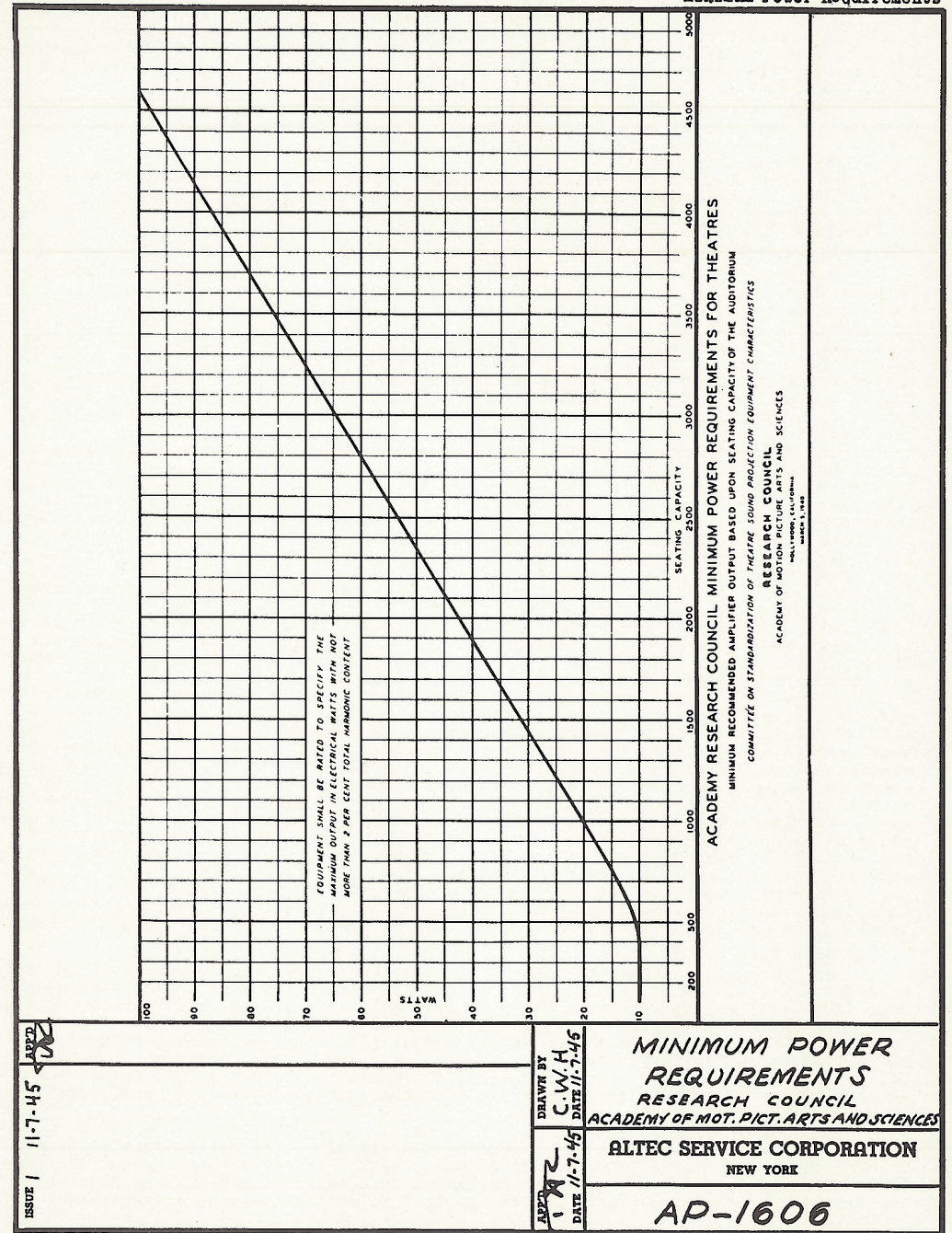
(a) The gain test may be thought of as separate from the frequency (8000 cps) response test. The only significance to this distinction is that a single frequency loop (1000 cps) may be used when the gain test only is required, with savings of time and inconvenience resulting thereby.

(b) Since the output of the PEC is a function of the polarizing voltage, the PEC voltage should be taken into account when considering the Variation from Normal Gain at the film amplifier input. This output variation is 0.1 to 0.2 db per volt above or below 90 volt. Also, extensive variations in the ac voltage will affect the characteristics of some amplifiers.

8. LIMITS - No definite limits have been set up for the intermediate points. Where two or more points are found to vary from normal, repairs or replacements should be made first at the point where the greater deviation is noted. It may then be found that the system is within acceptable limits and that no further changes are necessary.



Minimum Power Requirements



ISSUE 1 11-7-45

APPROVED BY [Signature] DATE 11-7-45

DRAWN BY C.W.H. DATE 11-7-45

MINIMUM POWER REQUIREMENTS  
RESEARCH COUNCIL  
ACADEMY OF MOT. PICT. ARTS AND SCIENCES

ALTEC SERVICE CORPORATION  
NEW YORK

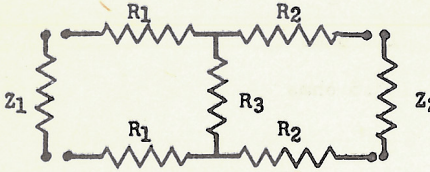
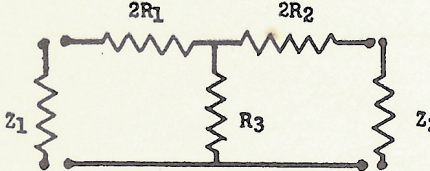
AP-1606







THE DESIGN OF ATTENUATION NETWORK

		TABLE NO. 1			
		LOSS DB	K <sub>3</sub>	K <sub>4</sub>	K <sub>5</sub>
 <p>H Type Pad</p>	1	4.34	4.34	1.013	
	2	2.21	2.15	1.05	
	3	1.51	1.43	1.12	
	4	1.16	1.05	1.23	
	5	.965	.82	1.37	
 <p>T Type Pad</p>	6	.835	.67	1.56	
	7	.725	.525	1.79	
	8	.690	.476	2.10	
	9	.645	.406	2.50	
	10	.610	.352	3.03	
	12	.565	.269	4.45	
	14	.540	.208	6.76	
	15	.532	.184	8.35	
	16	.525	.163	10.43	
	18	.515	.128	16.74	
		20	.510	.101	25.40
		25	.502	.056	79.80
		30	.500	.0318	247.00
	35	.500	.0178	784.00	
	40	.500	.0100	2401.00	
	45	.500	.00565	7921.00	
	50	.500	.00320	24964.00	

$$R_1 = (K_3 Z_1) - (K_4 \sqrt{Z_1 Z_2})$$

$$R_2 = (K_3 Z_2) - (K_4 \sqrt{Z_1 Z_2})$$

$$R_3 = 2 K_4 \sqrt{Z_1 Z_2}$$

The ratio ( $Z_1/Z_2$  or  $Z_2/Z_1$ ) of the larger terminal impedance of the pad to the smaller impedance cannot be greater than a quantity ( $K_5$  in Table No. 1) which depends upon the loss. The minimum matching loss will occur at the point where this ratio and  $K_5$  are equal in value.

**EXAMPLE:**

Design a 10 db pad working between a 400 ohm output and a 600 ohm input.

$Z_2/Z_1 = 600/400 = 1.5$  The combination is possible as  $K_5$  for 10 db loss is 3.03 which is greater than  $Z_2/Z_1$ . (Incidentally, a minimum loss pad for this ratio would be where  $K_5$  is equal to 1.5. Since 1.5 is not shown we will have to use the next larger number, or 1.56. The pad should be designed on the basis of 6 db loss.)

Then from Table No. 1 we see that for a loss of 10 db,

$$K_3 = 0.610$$

$$K_4 = 0.352$$



Substituting these and the given values of  $Z_1$  and  $Z_2$  we have,

$$R_1 = (.610 \times 400) - (.352 \times 490) = 71.5 \text{ ohms}$$

$$R_2 = (.610 \times 600) - (.352 \times 490) = 193.5 \text{ ohms}$$

$$R_3 = 2 \times .352 \times 490 = 345 \text{ ohms.}$$

In practice we would make,

$$R_1 = 70 \text{ ohms}$$

$$R_2 = 200 \text{ ohms}$$

$$R_3 = 350 \text{ ohms.}$$

(DON'T FORGET TO MULTIPLY  $R_1$  AND  $R_2$  BY TWO WHEN USED IN A "T" PAD. SEE SKETCH.)

NOTE:

The reader who is interested in the mathematical expressions will find a complete treatment of the subject in K.S. Johnson's "Transmission Circuits for Telephone Communication".